



**CONSTRUCTION EXPERIENCE**  
**AND**  
**DRILLED SHAFT INSTALLATION PLAN**  
**RENTON TO BELLEVUE, I-405 EXPANSION**  
**RENTON TO BELLEVUE, WA**

Submitted To:

**Flatiron**  
1400 Talbot Road, Suite 500  
Renton, WA 98055

Prepared By:

Michels Corporation  
8201 South 222<sup>nd</sup> Street  
Kent, WA 98032  
(253) 220-8004

I-405, Renton to Bellevue Widening & and Express Toll Lanes Project

**DOCUMENT REVIEW**

- ☒ APPROVED, NO EXCEPTION TAKEN
- ☐ APPROVED AS NOTED
- ☐ RESUBMIT, REVISE AS NOTED
- ☐ REVIEWED COMMENTS PROVIDED IF ANY

REVIEWED BY: Milan Radic, PE DATE: 11/16/21

Review is for general conformance with contract or design documents. Sole responsibility for correctness of dimensions, details, quantities, materials, and safety during fabrication and erection shall remain with the contractor

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## **SECTION A – DRILLED SHAFT FOUNDATIONS**

## **SECTION B – CONTRACTOR’S EXPERIENCE REQUIREMENTS**

### **SUB-ITEM (1): DRILLED SHAFT PROJECT EXPERIENCE**

Please find a list of drilled shaft projects completed by Michels Corporation attached in **Tab 1**.

### **SUB-ITEM (2): ON-SITE SUPERVISOR**

James Smith is the proposed Site Superintendent for the Drilled Shafts. Jarred Sedge is the proposed operator for the excavation crane. Resume for each of the above proposed personnel are attached in **Tab 2**.

## **SECTION C - SHAFT INSTALLATION PLAN**

The Geotechnical Data Report provided in the contract documents was prepared by WSDOT dated December 4, 2018. The bore logs were completed at various locations along the Right of Way (ROW) of the project.

The site soils generally consist of very loose to very dense silts, sands, and gravels. While class-conscious in some locations, many of the soil layers are a combination of the descriptions above with very little influence of water in most shaft locations and depths.

### **SUB-ITEM (1): OVERALL CONSTRUCTION SEQUENCE**

The general steps involved with the shaft construction are outlined below. Due to the soils represented in the Geotechnical Report, Michels intends to drill the sign shafts using Open Hole Drilling Methods. If required due to water infiltration, Michels will introduce slurry to maintain shaft wall stability.

#### **Open Hole Excavation Steps:**

1. Position the Drill rig on location and center the tooling in the correct location.
2. Begin excavation. Soil from within the shaft will be excavated with augers, digging buckets. Drill spoils to be deposited within swing radius of drill rig.
3. If required to maintain hole stability in the top 10’ of soils, Michels will install a temporary top casing.
4. Michels will continue the shaft excavation until the correct tip of shaft elevation is achieved.
5. After shaft is drilled to depth, the shaft will be cleaned with a spin bottom.

6. Pick drilled shaft cage and place in hole to the correct top and bottom of cage elevation.
7. Place tremie to the bottom of shaft prior to starting concrete placement.
8. Place concrete from bottom of shaft to top of shaft elevation.

**Slurry Shaft Excavation Steps:**

1. Position the Drill rig on location and center the tooling in the correct location.
2. Begin excavation. Soil from within the shaft will be excavated with augers, digging buckets. Drill spoils to be deposited within swing radius of drill rig.
3. If required to maintain hole stability in the top 10' of soils, Michels will install a temporary top casing.
4. As the excavation continues, slurry will be added to the shaft as required to provide and maintain hole stability below the previously placed top casing.
5. Excavate drilled shaft to depth using slurry drilling. During Excavation, a dedicated slurry crewmember will ensure a proper slurry head is maintained throughout the construction of the shaft.
6. After shaft is drilled to depth, the shaft will be cleaned with a spin bottom.
7. Pick drilled shaft cage and place in hole to the correct top and bottom of cage elevation.
8. After cleaning the base of the shaft and completing sand content test along with sounding bottom of shaft with weighted tape is complete, the concrete will be placed by the tremie method.
9. As concrete is placed in the shaft, the tremie will remain 5' – 10' in the concrete through the duration of the pour.
10. Finish concrete pour to top of shaft location.

**SUB-ITEM (2):      EQUIPMENT LIST**

The drilled shafts will be installed through a variety of soils in which promote open hole drilling or the use of slurry to maintain shaft stability. This NON-VIBRATORY method of drilled shaft construction reduces the potential for caving, bottom heave, and settlements. If hole stability is a concern, Michels will use drilling slurry to eliminate the potential for caving, heave, and settlement,

**Drill Rig 1:** Bauer BG-15 (for shafts 4' or smaller)



**Drill Rig 2:** Watson EX-130 (for shafts greater than 4')

**Support Crane:** Linkbelt TCC-500

**SUB-ITEM (3):        SHAFT EXCAVATION METHODS**

**SHAFT EXCAVATION METHODS – OPEN HOLE DRILLING**

The drilled shaft for open hole excavation will advance using a top drive rotary drill rig. The drill tools are equipped with carbide teeth that can penetrate most obstructions. If necessary, Michels will also have a core barrel on site to aid in removing challenging obstructions. After broken, the remains of the obstruction will be removed from bottom of the shaft with the core barrel or the digging bucket.

As the excavation begins, Michels will dig the shaft approximately 5' prior to installing a temporary top casing to maintain hole stability. The top casing will be installed from grade to approximately 10' below grade. After the top casing is installed, Michels will continue to drill below the bottom of the temporary top casing. Drilling will be advanced while depositing drill spoils within swing radius of the drill rig. As the excavation continues, a drill oiler, tied off to a Deadman, will be sounding the bottom of hole to confirm drill depth and ensure the shaft is not over drilled.

The dense moist geological conditions will lend themselves beneficial to open hole drilling conditions for the sign shafts. As the excavation advances, a Michels drill oiler will observe the soils being conveyed to surface to ensure they are representative of what is shown in the geotechnical report and suitable for open hole drilling.

**SHAFT EXCAVATION METHODS – SLURRY DRILLING**

Drilled shafts that will be excavated using a slurry drilling method using a conventional top drive drill rig. As the excavation is advanced, slurry will be placed into the drilled shaft to maintain the stability of the shaft. The drill tools are equipped with carbide teeth that can penetrate most obstructions. If necessary, Michels will also have a core barrel on site to aid in removing challenging obstructions. After broken, the remains of the obstruction will be removed from bottom of the shaft with the core barrel or the digging bucket.

As the excavation advances, a designated crewmember will monitor the slurry level to ensure hole stability. This crewmember will be responsible for continuously filling the shaft with slurry as the excavation advances. Additionally, another crewmember will be in charge of ensuring the slurry at the baker tanks is of adequate viscosity and cleanliness as it is conveyed to the drilled shaft.

Michels will do its very best to stop excavation at design tip elevation. To ensure a hard bottom, in a water head condition, Michels will perform a sand content test and sound bottom of shaft with a weighted tape, this will also be confirmed by an onsite inspector prior to

pouring. The pouring of a shaft will not occur until bottom of shaft is deemed sufficient. Michels will not use vibratory methods during shaft construction so liquefaction will not occur.

During the shaft excavation the drill spoils will be loaded directly into trucks a spoils box or ground adjacent to shaft for removal from site and disposal.

#### **SUB-ITEM (4):        METHODS TO ENSURE SHAFT STABILITY**

##### **OPEN HOLE DRILLING:**

As stated above, Michels will only employ open hole drilling methods should the soil conditions be appropriate. If the soil conditions consist of medium to dense well graded soils with the absence of ground water, Michels will use open hole drilling methods.

To maintain top of hole stability, and prevent cave-ins, michels will use a temporary top casing that will extend approximately 10' below grade. Michels will then use open hole drilling methods to advance the shaft beyond the tip of the temporary casing. As the excavation advances, the drill oiler will monitor the drill spoils conveyed out of the shaft to ensure they are representative of what is shown in the geotech report.

Should Michels enter into soils not capable of standing freely without additional shaft stabilization, Michels will use slurry drilling methods to complete the remainder of the shaft. Michels will have slurry on site in case an unforeseen soil condition is encountered and need to flood the hole.

##### **SLURRY DRILLING:**

Shafts to be constructed in unstable soils will require polymer slurry to maintain hole stability during excavation and concrete placement. As the excavation advances, Michels will have a dedicated crewmember to ensure the proper amount of slurry is introduced into the shaft to maintain adequate head pressure. Additionally, Michels will have a certified slurry technician at the baker tank to monitor the cleanliness and viscosity of the slurry. Upon reaching tip elevation, Michels will measure the fine content to ensure there is less than 1 percent of suspended fines. If the slurry needs to be cleaned, Michels will floc the hole with approved flocculant.

After the shaft has been cleaned and ready to be poured, Michels will place approximately 10' of concrete in the bottom of the shaft prior to lifting the tremie. After 10' of concrete has been placed, the tremie will be raised at the same pace as the concrete. At no point will the tremie be pulled out of the concrete until final top of shaft elevation is achieved.

**SUB-ITEM (5):            SLURRY METHODS**

For Slurry shafts, Michels will use Shore Pac Polymer Slurry by Cetco. Shore Pac Slurry has been recommended for this project due to its versatility and success in similar ground conditions to be found on site. Where Michels will use slurry drilling methods, it is expected to find, gravels, sands, and silts. Shore Pac is an environmentally slurry and readily recycled for the use on subsequent shafts. Additional information about Shore Pac can be referenced on **Tab 2**.

During slurry drilling operations, Michels will have a certified slurry technician monitoring the viscosity and cleanliness of the slurry. When using slurry on site, it is Michel's intention to mix the slurry in a baker tank prior to deploying in the shaft. Due to the geotechnical conditions found on site, it is estimated the viscosity of the slurry to be used on site will be 100-130 seconds per quart. This is monitored in all outgoing tanks during drilling operations.

As the excavation advances, Michels will have a dedicated employee that will monitor the level of slurry inside the drilled shaft. This employee will communicate directly with the driller and the slurry technician at the tank farm. Slurry will be continuously added during the excavation until tip of shaft elevation is achieved.

After the drilled shaft has been cleaned, concrete placement will commence. During concrete placement, Michels will pump the used slurry back to the tank farm to settle and be recycled for other shafts. This slurry will be recycled until it is no longer suitable to use.

Once the slurry is dead (lost viscosity), Michels will kill the PH level using soda ash. Once the PH level is within a tolerable range, and suspended particles have dropped out of the water, the drill water will be pumped to a discharge point provided by others.

**SUB-ITEM (6):            QUALITY CONTROL PLAN FOR SLURRY**

The Michels Slurry technician on site is in charge of the quality of the slurry pumped in and out of the drilled shafts. Water used to create slurry on site must be clean, low in chorine, and no grey water.

Tools on site to monitor slurry:

1. **Mud Density Weight** – 64 Lb/ft<sup>3</sup>
2. **Marsh Funnel** – Target Viscosity 100-130
3. **PH Strips** – 8.5-9.5
4. **Sand Content Test Kit** – Less than or equal to 1%

Each of these tools will be used to monitor new slurry being created in baker tanks, recycled slurry in baker tanks, and in the drilled shaft. Michels will also be using diaphragm water

pumps (screwsuckers) because they don't "chop" the slurry when conveyed to and from the shaft. This lends to a higher quality product with a longer lifespan.

**SUB-ITEM (7):            METHOD TO ELIMINATE VOIDS**

Prior to the installation of the drilled shafts, the earthwork contractor will cut grade down to top of shaft elevation to eliminate voids at the top of shaft elevation. Should the top of shaft be below grade, a temporary CMP pipe will be installed by others to create a clean transition at the top of sign shaft.

**SUB-ITEM (8):            REINFORCING STEEL SHOP DRAWINGS**

Reinforcing cage shop drawings, fabrication and supply are the responsibility of the General Contractor and shop drawings will be submitted by them under separate cover.

Reinforcing cages as specified in the Contract Documents are to be delivered to the jobsite pre-tied (or tied on-site, as working area permits) and placed by Michels into the individual drilled shaft after the shaft has been drilled to the final tip elevation.

Cages are to be properly cross-braced such that cage deformation does not occur during the lifting, handling and placement operation. The cages are to be properly rigged such that they can be lifted from a horizontal position to a vertical position without compromising the integrity of the cage and/or the hoisting/rigging equipment. Centralizing devices are tied to the vertical and/or spiral bars of the cages prior to hoisting of the cage.

During final placement of shaft cages 4 each nylon slings will be placed at equal spacing around the shaft change. The chains will be attached to a spreader bar held by the hook of the crane.

**SUB-ITEM (9):            CONCRETE PLACEMENT METHODS**

After an individual shaft has been excavated to the designed depth and the base of the shaft has been cleaned; any fine materials suspended in the water (if excavated under water) will be removed from the bottom of the shaft. If water is present, a sand content test will be performed to test the water at both the bottom and at mid-height prior to the concrete placement operation commencing work.

Concrete is to be placed using a boom pump attached to a 4"-5" diameter tremie pipe (slick line) that extends to the full length of the shaft. A seal or plug (commonly referred to as a "pig" or "rabbit") is placed into the top of the tremie pipe. Concrete is then pumped through the tremie pipe continuously with a minimum of 10' of head maintained above the bottom of the tremie pipe. The high slump concrete will freely flow around the steel reinforcement and against the soil face filling any pockets or voids that exist. For this reason, and due to the properties of the high slump concrete vibrating of the concrete is not necessary in any portion of the shaft.

While the shaft is pumped with concrete from the bottom up, Michels will keep a 10' concrete head from top of concrete to bottom of tremie until top of shaft is achieved. This is to ensure proper concrete placement and that concrete completely flows around the drilled shaft cages and against the soil face.

The Concrete Mix Design for the shafts is attached under **Tab 5**. This concrete mix has proven itself to be superior for construction of drilled shafts utilizing open hole and slurry drilling methods.

**SUB-ITEM (10): UNPLANNED PAUSES OR STOPS AND EMERGENCY CONSTRUCTION JOINTS**

For unplanned pauses or stops in work during the excavation operation, due to Michels employing an open hole and slurry drilling methods the following will take place:

1. Any drilled shaft will not be left for greater than 14 hours without a michels employee monitoring the hole. If required to sit greater than 14 hours, Michels will fill the shaft with slurry and monitor every 24 hours.
2. Should the shaft require Michels to be down greater than 48 hours due to an unplanned stop or emergency, Michels will backfill the shaft with a pumpable lean mix for a re-drill at a later date.

If a problem is encountered in the lower portion of the shaft during a concrete pour and a joint is required the concrete and re-steel will be removed from the shaft and the pour started over at a later date. If an emergency joint is required in the upper portion of the shaft and it is not practical to remove the concrete and re-steel then after the concrete has set, the surface of the concrete will be cleaned and the laitance removed and the concrete pour will be re-started.

**SUB-ITEM (11): UNAUTHORIZED ENTRY DEVICES**

During work hours, Michels will supervise its own personnel and activities in proximity of the shaft. During non-working hours, the General Contractor is responsible for securing the general work site. Any open shafts are to be covered and secured to prevent any unauthorized entry, usually with plywood or steel plate, then if required a piece of construction equipment or another heavy object placed on top to prohibit removal of the shaft cover.

**SUB-ITEM (12): NONDESTRUCTIVE TESTING**

There will be no nondestructive testing for the sign shafts.



**TAB 1**

# Reference/Experience List



## Drilled Shafts

Year	Owner/Customer	Contact	Phone Number	Project Name	Description / Foundation Type	Location	Contract Value	Status
2021	HP Civil	Josh Smith		Southern Oregon Seismic	Install 144 EA micropiles, 162 EA ground anchors and 12 EA - 72" DIA drilled shafts	Grants Pass, OR	\$2,659,600.00	
2020	Strider	Kyle Gebhardt	360-380-1234	Thornton Overpass	Install 140 LF of 6' DIA shafts, 480 LF of 8' DIA shafts	Ferndale, WA	\$798,500.00	
2020	Flatiron	Joseph Okelberry	425-420-9982	I-405 Renton to Bellevue	Install 246 EA drilled shafts ranging from 3' DIA to 8' DIA and 902 EA - 2.5' noise wall shafts	Renton, WA	\$10,898,260.92	
2020	Atkinson			SR 3 Chico Creek	20,000 SF shotcrete install, soil nail, 22 EA 3.28' DIA, 8 EA 3.92' DIA Drill shaft install, 10 EA 6.56" DIA, 10 EA 8.2' DIA Drill Shafts	Bremerton, WA	\$1,710,162.00	
2020	Walsh	Ben Mitchel		Union Street Ped Bridge	Install 15 EA micropiles and 8 EA drilled shafts ranging in DIA between 1.2M - 2.2M	Seattle, WA	\$571,697.61	
2020	IMCO	Brett Himes	360-671-3936	Mukilteo Ferry Terminal Phase 2	Install 15 EA micropiles and 8 EA drilled shafts ranging in DIA between 1.2M - 2.2M	Mukilteo, WA	\$165,206.00	
2020	Kiewit	Wes Renton	808-753-0406	Federal Way Link Ext	2.5', 3.0", 4.92', 8.2' 9.19', 9.84', 11.25' DIA shafts, shaft spoil removal, and top casings	Federal Way, WA	\$17,996,456.00	
2020	RL Wadsworth	Jon Lowe	801-553-1661	Porter Rockwell	Install 4 EA - 2.5M shafts	Draper, UT	\$595,176.00	
2020	Granite/RLW	Derek Harames	801-533-1661	US-89 to I-84	Install 32 EA drilled shafts ranging from 1M DIA - 2M DIA	Layton, UT	\$851,162.00	
2020	Wadsworth Bros	Linn Bogart	435-218-3948	BBP Yellowstone	236 EA 6' DIA, 562 EA 10' DIA drilled shaft, concrete and 10 EA themral integrity	Billings, MT	\$1,571,399.00	
2020	Turner	Matt Bystedt	206-391-9997	1400 Madison	Install 61 EA soldier piles, 4,485 SF of lagging, 9 EA - 1.5M drilled shafts and 25 EA - 1M drilled shafts	Seattle, WA	\$1,092,801.00	
2020	Sletten	Russell Robertson	406-868-7429	Higgins Ave	Install 1 EA - 3' DIA drilled shaft and 9 EA - 4' DIA drilled shaft	Missoula, MT	\$248,388.00	
2020	Selland	James Flowers	509-881-0339	Easton Hill	Install 10 EA - 4' DIA drilled shafts	Easton, WA	\$400,623.00	
2020	Garco Construction	Tim Hutton	509-535-4688	Spokane River Bridge Trent Ave	Secant Piles and Drilled Shafts (8 & 10' dia)	Spokane, WA	\$1,419,200.00	
2020	Hamilton Construction	Joe Hampton	541-746-2426	OR38 Umpqua River Bridge	Permanent Shoring and Drilled Shafts (8' dia)	Scottsburg, OR	\$2,450,000.00	
2020	Highmark	John Harris	360-829-5189	Issaquah Fall City Road	Install 6 EA - 2.5M DIA and 6 EA - 3M DIA drilled shafts and 302' slip casing	Issaquah, WA	\$841,527.00	
2020	Halme	Seth Ritter	509-725-4200	BNSF Realignment	Install 8 EA - 3' and 32 EA - 4' DIA drilled shafts	Spokane, WA	\$798,293.30	
2019	Granite	Vance Aeschleman	425-508-6002	Waterfront Seattle Alaskan Way	31 EA between 1.2M, 2M, 2.8M and 3M DIA drilled shafts	Seattle, WA	\$2,821,923.00	
2019	Granite	Blake Ambler	425-754-2235	East of Elgin Clifton	4 EA - 2M DIA drilled shafts	Pierce County, WA	\$405,096.00	
2019	IMCO	C Masek	425-452-6800	Mountains to Sound	2 EA - 1.2M and 4 EA - 2.5M DIA drilled shafts, 182 soldier piles, 243 DCP tiebacks and 22,545 SF lagging	Bellevue, WA	\$2,611,000.00	
2019	Mortenson	Tony Munoff	425-497-7199	Citizen M	24 EA - 1.2M drilled shafts and 37 EA well point dewatering well	Seattle, WA	\$631,577.00	
2019	SWK	Landon Lovingfoss	503-381-1704	Redmond Link Extension	Drilled shafts ranging from 10 EA - 4' DIA, 15 EA - 5' DIA, 5 EA - 6' DIA 20 EA - 8' DIA, 22 EA - 9' DIA and 2 EA - 10' DIA and installation of permanent casing	Redmond, WA	\$7,151,242.00	
2019	Quigg Brothers	Ben Jones	360-533-1530	West Jefferson County	Install drilled shafts ranging from 4 EA - 1.5M DIA, 6 EA - 2M DIA, 4 EA - 2.5M DIA and 18 EA soldier piles	West Jefferson County, WA	\$2,022,716.00	
2019	Interwest Construction	Jordan Ter Har	360-899-2013	Sultan River Bridge	7 EA - 2m DIA drilled shafts and installation of permanent casing	Sultan, WA	\$375,822.00	
2019	Atkinson	Ryan Cearly	425-757-6549	I-5 Portland Ave SB	33 EA drilled shafts between 2M and 3M DIA, permanent/temporary/slip casing, 1,470 EA temporary soil nails and 35,578 SF of shotcrete	Tacoma, WA	\$6,236,192.00	
2018	Michels Pipeline	Will Foster	253-332-2857	Tolt Bridge	Drill 8 caissons 24" DIA, 31.7' deep. Install casing through 15' of overburden and the water table into glacial material. Install cages and 4000 psi concrete in shafts.	Woodinville, WA	\$138,295.00	

**MICHEL'S®**

**FOUNDATIONS**



**TAB 2**



### PROFESSIONAL EXPERIENCE

#### 2019 – Present: Foreman | Michels Corporation | Kent, WA

Supervised construction projects from beginning to end and coordinated workers. Responsible for guiding staff, overseeing concrete installation, assigning tasks, preventing occupational hazards, and keeping records. Demonstrated technical skills, managerial abilities, attention to details, stamina, basic computer operation knowledge, and teamwork.

### PROJECT PROFILES

Granite Construction | SR11 Padden Creek; Install 82 EA soldier piles, 212 ground anchors and 18,300 SF of lagging – Bellingham, WA

Tapani | PLW 1.3; Launch Pit Shoring and Receiving Shaft Shoring  
– Beaverton, OR

IMCO | Mukilteo Ferry Terminal; 30" DIA Shafts, 14x120 LF Soldier Pile, 1180SF lagging  
– Mukilteo, WA

Kiewit | Federal Way Link Ext; 2.5' , 3.0", 4.92', 8.2' 9.19', 9.84', 11.25' DIA shafts, shaft spoil removal, and top casings – Federal Way, WA

BNBuilders | Building X; Install 256 EA soldier piles, 159 EA tiebacks, 28,382 SF of lagging, 41,035 LF of rigid inclusions – Redmond, WA

Rodarte | S 180th Street; Well point well installation, discharge, removals & mobilization  
– Auburn, WA

Holland Partners | Block 10; Temporary shoring (soldier piles / tiebacks / lagging)  
– Vancouver, WA

Granite | 520 Trail; 144 total permanent soldier piles and lagging  
– Redmond, WA

Garco Construction | Spokane River Bridge Trent Ave.; Secant Piles and Drilled Shafts (8 & 10' dia)  
– Spokane, WA

SWK | Redmond Link Extension; Drilled shafts ranging from 10 EA - 4' DIA, 15 EA - 5' DIA, 5 EA - 6' DIA 20 EA - 8' DIA, 22 EA - 9' DIA and 2 EA - 10' DIA and installation of permanent casing  
– Redmond, WA

IMCO | Mountains to Sound; 2 EA -1.2m and 4 EA - 2.5m DIA drilled shafts, 182 soldier piles, 243 DCP tiebacks and 22,545 SF lagging  
– Bellevue, WA

Highmark | Issaquah Fall City Road; Install 6 EA - 2.5m DIA and 6 EA - 3M DIA drilled shafts and 302' slip casing  
– Issaquah, WA

Granite | East of Elgin Clifton; 4 EA - 2m DIA drilled shafts  
– Pierce County, WA

## PROJECT PROFILES (continued)

Turner | Waverly (210- 8th); 97 EA soldier piles backfilled with concrete and lean mix, 303 EA tiebacks, 48 tie rods and 28,651 SF wood lagging

— Seattle, WA

Greystar | Arista U-Village; 463 Pressed permanent sheet piles, 114 temporary tiebacks, waler for sheet piles and tiebacks, 502 auger cast piles, removal or water system, 12 deep dewatering wells and 12 smart dewatering boxes to regulate flow rates

— Seattle, WA

Rodarte | Foothills Trail;

2019 Rodarte Foothills Trail 315 EA soil nail, 5,162.5 SF of 4" shotcrete

— Enumclaw, WA

Garco Construction | Cle Elum Gate; 114 EA soldier piles, 412 EA tiebacks and 34,650 SF of lagging

— Cle Elum, WA

Atkinson | i-5 Portland Ave SB; 33 EA drilled shafts between 2m and 3m DIAM, permanent/temporary/slip casing, 1,470 EA temporary soil nails and 35,578 SF of shotcrete

— Tacoma, WA

Walsh | Denny Way Substation; 391 Soldier Piles, 25,800 sq. ft. of lagging, and 130 tiebacks. — Seattle, WA

Graham | 1st Denny Lofts ; 13 Soldier piles, 26 tiebacks, 381 Soil nails, 31,000 sq. ft. shotcrete, and 8900 sq. ft. lagging. — Seattle, WA

City of Redmond | 360 Eastlink; 31- 30" DIA drilled shafts — Redmond, WA

Granite | College Way Marysville; 61 Tiebacks, 19,000 sq. ft. shotcrete placed. — Marysville, WA

Granite | 116th Overpass; 15 - 3.0 M shafts, 17 - 2.5 M shafts — Marysville, WA

Petra Construction | Assisted Living Apartments; 36 Soldier piles, soil nails, 9000 sq. ft. shotcrete placed. — Issaquah, WA

City of Issaquah | Road Improvement; 26 can levered soldier piles, 10,119 sq. ft. of lagging — Issaquah, WA

Absher | Annie Wright School for boys and gym; 9 under pinned Piles, 50 Soldier piles installed, 124 Tiebacks installed, and 28,756 sq. ft. lagging — Tacoma, WA

## TRAINING & CERTIFICATIONS

- Pilot Escort - Washington State
- ACI certified Nozzleman (Vertical Only)
- Erosion and Sediment Control Lead Certified
- Trenching Excavating Competence
- Forklift Certification
- First Aid/CPR/AED Certification
- Flagger Certified
- Rigging Training
- Confined Space Entry Training

### PROFESSIONAL EXPERIENCE

#### Drill Operator | Michels Corporation | Kent, WA

Duties include set up drill and support equipment so that foundation investigations can be accomplished by directing the moving of equipment onto the site; arranging equipment within work area. Operate drill rigs to obtain undisturbed soil samples and ground water information so that parameters can be selected for foundations design by choosing and mixing correct types and viscosity of drilling fluids. Responsible for daily inspection for the daily inspection reports and daily preventative maintenance of the equipment.

### PROJECT PROFILES

Granite Construction | SR11 Padden Creek; Install 82 EA soldier piles, 212 ground anchors and 18,300 SF of lagging with permanent ground anchors

— Bellingham, WA

Tapani | PLW 1.3; Launch Pit Shoring and Receiving Shaft Shoring

— Beaverton, OR

Hamilton Construction | OR38 Umpqua River Bridge ; Permanent Shoring and Drilled Shafts (8' dia)

— Scottsburg, OR

SWK | Redmond Link Extension; Drilled shafts ranging from 10 EA - 4' DIA, 15 EA - 5' DIA, 5 EA - 6' DIA 20 EA - 8' DIA, 22 EA - 9' DIA and 2 EA - 10' DIA and installation of permanent casing

— Redmond, WA

Michels Pipeline | Jackson Prairie (Saturn Centaur Filter Separator Installation); Micropiles — Lewis County, WA

Rodarte | Foothills Trail; 315 EA soil nail, micro piles, and 5,162.5 SF of 4" shotcrete

— Enumclaw, WA

Turner | 1400 Madison; Install 61 EA soldier piles, 4,485 SF of lagging, 9 EA - 1.5M drilled shafts and 25 EA - 1M drilled shafts

— Seattle, WA

BNBuilders | Building X; Install 256 EA soldier piles, 159 EA tiebacks, 28,382 SF of lagging, 41,035 LF of rigid inclusions

— Redmond, WA

Holland Partners | Block 10; Install 45 EA soldier piles, 38 EA tiebacks and 5,415 SF of lagging

— Vancouver, WA

Granite | 520 Trail ; 144 total permanent soldier piles and lagging

— Redmond, WA

IMCO | Mountains to Sound; 2 EA -1.2M and 4 EA - 2.5M DIA drilled shafts, 182 soldier piles, 243 DCP tiebacks and 22,545 SF lagging with permanent ground anchors

— Bellevue, WA



**PROJECT  
PROFILES**  
(continued)

Granite | East of Elgin Clifton; 4 EA - 2M DIA drilled shafts

— Pierce County, WA

Kiewit | Federal Way Link Ext; 2.5' , 3.0", 4.92', 8.2' 9.19', 9.84', 11.25' DIA shafts, shaft spoil removal, and top casings

— Federal Way, WA

Turner | Waverly (210 8th); 97 EA soldier piles backfilled with concrete and lean mix, 303 EA tiebacks, 48 tie rods and 28,651 SF wood lagging

— Seattle, WA

GreyStar | Arista U-Village; 463 pressed permanent sheet piles, 114 temporary tiebacks, waler for sheet piles and tiebacks, 502 augercast piles, removal or waler system, 12 deep dewatering wells and 12 smart dewatering boxes to regulate flow rates

— Seattle, WA

Granite | Waterfront Seattle Alaskan Way; 31 EA between 1.2M, 2M, 2.8M and 3M DIA drilled shafts

— Seattle, WA

Garco Construction | Cle Elum Dam; 114 EA soldier piles, 412 EA tiebacks and 34,650 SF of lagging with permanent ground anchors

— Cle Elum , WA

Atkinson | I-5 Portland Ave SB; 33 EA drilled shafts between 2M and 3M DIA, permanent/temporary/slip casing, 1,470 EA temporary soil nails and 35,578 SF of shotcrete

— Tacoma, WA

**TRAINING &  
CERTIFICATIONS**

- OSHA 10-hour Construction
- Forklift Training Certification
- Confined Space Awareness
- Rigging Training
- First Aid/CPR/AED Certification

**MICHEL'S®**

FOUNDATIONS



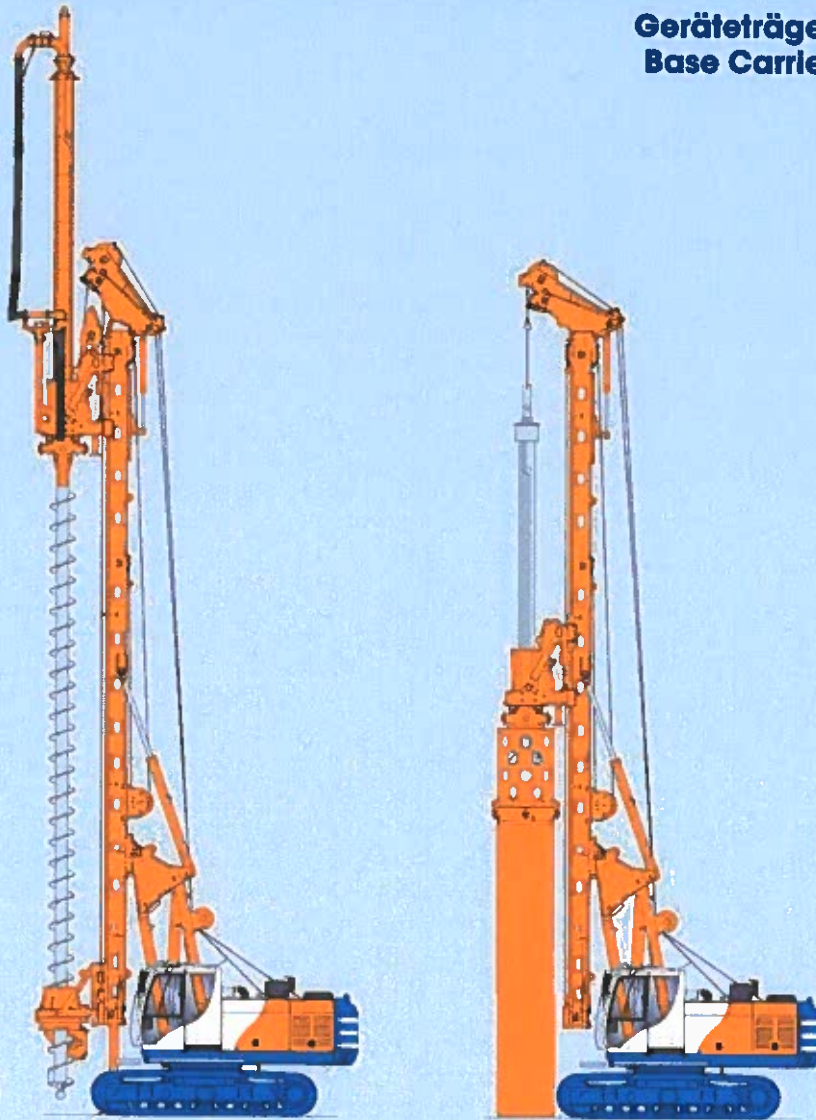
**TAB 3**

# BAUER BG 15 H

Großdrehbohrgerät  
Rotary Drilling Rig

*PremiumLine*

Geräteträger BT 40  
Base Carrier BT 40





Die **BG 15 H**, ein Gerät mit einem Einsatzgewicht von ca. 49 to dient zur Herstellung von

- verrohrten Bohrungen (Eindrehen des Bohrohres mit dem Drehgetriebe oder mit angebauter Verrohrungsmaschine)
- unverrohrten, flüssigkeitsgestützten Bohrungen
- Bohrungen mit langer Hohlschnecke (SOB) - mit oder ohne Kellyverlängerung
- Sonderverfahren wie VdW-Bohren, Verdrängerbohrungen

The **BG 15 H** rotary drilling rig has an operating weight of approx. 49 to. It is ideally suited for:

- Drilling cased boreholes (installation of casing by rotary drive or optionally by hydraulic oscillator – both are powered by the drilling rig)
- Drilling uncased deep boreholes that are stabilised by drilling fluids
- Drilling boreholes with long hollow stem augers (CFA system), with or without kelly extensions
- Special drilling systems, such as FOW piles, displacement piles

## Bohrverfahren mit Serienausstattung:

Kellybohren (ohne Verrohrungsmaschine)

SOB-Verfahren (hydraulisch und elektrisch vorgerüstet)

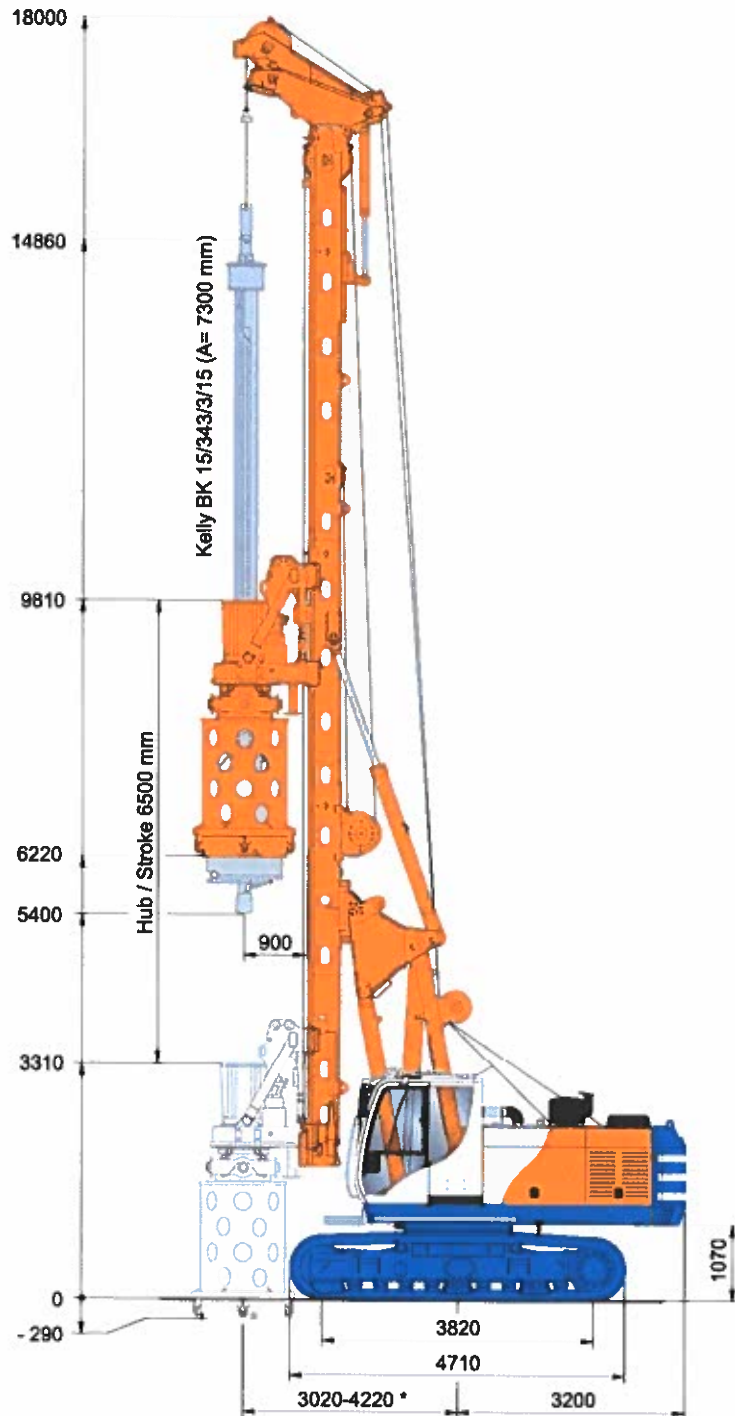
FDP Verdrängerbohren (hydraulisch und elektrisch vorgerüstet)

## Drilling processes with standard equipment:

Kelly drilling (without casing oscillator)

CFA drilling (pre-equipped with hydraulic and electric installations)

FDP Full-Displacement-Piling (pre-equipped with hydraulic and electric installations)



\* Horizontalverschiebung (abhängig von der Bohrausrüstung)  
horizontal mast reach (depending on the drilling equipment)

## Technische Daten

## Technical data

<b>Gesamthöhe</b>	<b>Overall height</b>	<b>18.000 mm</b>
<b>Einsatzgewicht ca. (mit Kelly BK15/343/3/15)</b>	<b>Operating weight (approx.) (with Kelly BK15/343/3/15)</b>	<b>49.000 kg</b>
<b>Drehantrieb</b>	<b>Rotary drive</b>	<b>KDK 150 KL</b>
Drehmoment (nominal) bei 300 bar	Torque (nominal) at 300 bar	151 kNm
Drehzahl max	Speed of rotation (max.)	36 U/min (RPM)
<b>Vorschubwinde</b>	<b>Crowd winch</b>	
Druckkraft / Zugkraft (effektiv)	Crowd pressure push / pull (effective)	200 / 200 kN
Druckkraft / Zugkraft gemessen am Drehteller KDK	Crowd pressure / pull measured at the casing drive adapter on the rotary drive	150 / 150 kN
Hub (Kellysystem)	Stroke (kelly system)	6.500 mm
max. Schlittenhub	max. stroke of sledge	12.600 mm
Geschwindigkeit (ab/auf)	Speed (down/up)	7,0 / 7,0 m/min
Schnellgang (ab/auf)	Fast speed (down/up)	27 / 27 m/min
<b>Hauptwinde</b>	<b>Main winch</b>	
Windenklasse	Winch classification	M6 / L3 / T5
Zugkraft (1. Lage effektiv)	Single line pull (1 <sup>st</sup> layer effective)	110 kN
Zugkraft (1. Lage nominal)	Single line pull (1 <sup>st</sup> layer nominal)	140 kN
Seildurchmesser	Rope diameter	22 mm
Windengeschwindigkeit	Line speed max.	77 m/min
<b>Hilfswinde</b>	<b>Auxiliary winch</b>	
Windenklasse	Winch classification	M6 / L3 / T5
Zugkraft (1. Lage effektiv)	Single line pull (1 <sup>st</sup> layer effective)	55 kN
Zugkraft (1. Lage nominal)	Single line pull (1 <sup>st</sup> layer nominal)	70 kN
Seildurchmesser	Rope diameter	15 mm
Windengeschwindigkeit	Line speed (max.)	55 m/min
<b>Mastneigung</b>	<b>Mast inclination</b>	
nach hinten / vorne / quer	Backward / forward lateral	15° / 5° / + - 5°

## Bohrgerät

## Drilling rig

### Serienausstattung

- Drehgetriebe KDK 150 KL (Konstantgetriebe)
- Hauptwinde mit hydraulischer Freilaufsteuerung
- Haupt- und Hilfswinde mit Spezialrillung
- Hubendschalter für Haupt- und Hilfswinde
- Wirbel für Hauptseil
- Vorschub schnell / langsam
- Schwenkbarer Anschlagpunkt für Haupt- und Hilfsseil
- Elektronisch kontrollierte Horizontalverschiebung

### Zusatzausstattung

- Wirbel für Hilfsseil
- Mastabstützung
- Kellyablage
- obere Kellyführung für Kellystange BK 200/368
- Zusatzhilfswinde 20 kN
- Zentralschmierung
- Kameraanbau
- Betonierleitung
- Mechanische Anbauten für Automatikdrehteller
- Hydraulische Vorbereitung für Schneckenputzer
- Verrohrungsmaschinenanbau (max. BV 1300 L-03)
- Gittermastverlängerung (für HDI)
- Anbau für Tiefenrüttler TR 17

### Standard equipment

- Rotary drive KDK 150 KL (single gear drive)
- Main winch with hydraulically operated freewheeling
- Main and auxiliary winch with special grooving
- Hoist limit switch on main and auxiliary winches
- Swivel for main rope
- Crowd in fast or slow mode
- Pivoted anchor points for main and auxiliary ropes
- Electronic controlled horizontal mast reach

### Optional equipment

- Swivel for auxiliary rope
- Mast support unit
- Kelly transport support
- Upper kelly guide for kelly bar BK 200/368
- Additional auxiliary winch 20 kN
- Central lubrication system
- Video camera attachment
- Concrete line
- Mechanical attachment for automatic casing drive adapter
- Hydraulic preparation for auger cleaner
- Oscillator attachment (max BV 1300 L-03)
- Lattice mast extension (for Jet Grouting)
- Attachment for depth vibrator TR 17



## Mess- und Steuerungstechnik

### Serienausstattung

- Komfortpaket
  - Hauptwinde mit elektronischer Seilkraftmessung
  - Schlappseilabschaltung Hauptwinde
  - Funktion "Wirbel Aufstellen" Hauptwinde
  - Drehzahlmessung KDK
  - Anpressdruckregelung Kelly
  - Vorschubgeschwindigkeitssteuerung
  - Überlastschutz für Hauptseil
  - Überwachung Endscharter / Sensorik
- B-TRONIC 3.1 elektronisches Steuerungs-, Kontroll-, und Visualisierungssystem
- SPS Rechner für alle elektrisch angesteuerten Funktionen
- Integrierter Farbbildschirm zur Anzeige der Gerätedaten
- Anzeige von Fehlermeldungen in Klartext
- Notsteuerung Bohrergerät (Kernfunktionen)
- Mastneigungsmessung in x/y Richtung
- Mastautomatik (automatische Vertikalstellung)
- Hilfswinde mit hydraulischer Seilkraftmessung
- Tiefenmessung Hauptwinde
- Wegmessung Vorschubwinde
- Schockiereinrichtung für KDK
- Aufzeichnung und Fernübertragung der Betriebsdaten mit DTR-Modul

### Zusatzausstattung

- Kellyvisualisierung für Kellystange BK 200/368
- Hilfswinde mit elektronischer Seilkraftmessung
- Abbohr- und Ziehassistent für 'Single Pass' Verfahren

## Measuring and control equipment

### Standard equipment

- Comfort package
  - Electronic load sensing on main rope
  - Rope slack prevention on main winch
  - Swivel alignment function on main winch
  - Speed measuring device on KDK
  - Crowd pressure control for Kelly
  - Crowd speed control
  - Overload protection device on main rope
  - Automatic control of end switches and sensors
- B-TRONIC 3.1 Electronic monitoring-, control- and visualization- system
- PLC processor for all electrically actuated functions
- Integrated colour monitor for displaying machine operating data
- Display of fault messages as plain text
- Emergency mode of operation for drilling rig (core functions)
- Mast inclination measurement on x/y axes
- Automatic vertical alignment of mast
- Hydraulic load sensing on auxiliary rope
- Depth measuring device on main winch
- Distance measuring device on crowd winch
- Uni-directional impact function on KDK (for auger discharge)
- Recording and remote transmission of operating data with DTR-module

### Optional equipment

- Kelly visualization for Kelly bar BK 200/368
- Electronic load sensing on auxiliary rope
- Crowd control assistance and tool extraction assistance for 'Single Pass' application

## Trägergerät

### Serienausstattung

- Motornotsteuerung
- Leerlaufautomatik (zur Verbrauchsoptimierung)
- Motordiagnostiksystem
- Diagnoseleiste für hydraulische Funktionen
- abnehmbarer Ballast
- Verzurraugen an Raupenträgern
- Aufstiegsleiter zum Oberwagen
- Bordbeleuchtungssatz
- Bordwerkzeugsatz
- Elektrische Betankungspumpe
- Moderne, ergonomische Fahrerkabine mit FOPS Standard
- Klimaanlage
- Radio mit CD, MP3, USB und Bluetooth-Freisprecheinrichtung
- Trittraste neben der Kabine
- Dachschutzgitter
- 2 Kameras zur Rückraumüberwachung

### Zusatzausstattung

- Kompressor (1000 l/min Saugleistung)
- Generator 13 kVA
- Zusatzballast 2,25 t
- Bioölbefüllung
- Standheizung mit Zeitschaltuhr
- Trittraste oder Werkzeugkasten vor Kabine
- Frontschutzgitter
- Klimaautomatik (Climatronic)
- Kältepaket
- Absturzsicherung am Oberwagen
- Arbeitsscheinwerfer LED

## Base carrier

### Standard equipment

- Emergency mode of operation for engine
- Automatic idling mode (to optimise fuel consumption)
- Engine diagnostic system
- Diagnostic panel for hydraulic functions
- Removable counterweight
- Transport securing lugs on crawler units
- Access ladder on uppercarriage
- On-board lighting set
- On-board tool set
- Electric refuelling pump
- Modern, ergonomic operator's cab, FOPS compliant
- Air conditioning system
- Radio with CD, MP3, USB and Bluetooth c/w hands-free kit
- Catwalk on side of operator's cab
- Protective roof guard
- 2 cameras for rear area surveillance

### Optional equipment

- Compressor (1000 l/min capacity)
- Electric generator 13 kVA
- Additional counterweight 2.25 to
- Bio-degradable oil
- Independent cab heater with clock timer
- Catwalk or tool box in front of cab
- Front screen guard
- Climatronic
- Arctic kit
- Guardrails upper level
- LED spotlights

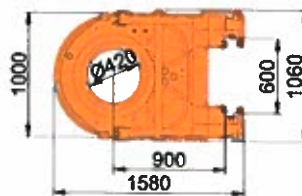
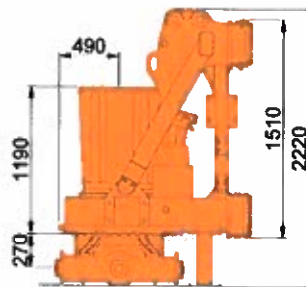
## Konstantgetriebe KDK 150 KL

### Serienausstattung

- Gleitleisten sind ohne Demontage des Drehgetriebes auswechselbar
- Auswechselbare Mitnehmerleisten
- Kardangelen
- Hydraulische Verbindungen mit Schnellkupplungen
- 3 einstellbare Betriebsmodi: (siehe Diagramme)
- Transportstützen
- Hebegeschirr

### Zusatzausstattung

- Kellyausrüstung KA 420/368



Gewicht mit Schlitten 3,7 t  
Weight with sledge

## Single gear rotary drive KDK 150 KL

### Standard equipment

- Wear pads exchangeable without removal of rotary drive
- Exchangeable kelly drive keys
- Cardanic joint
- Quick-release couplers on hydraulic hoses
- 3 selectable modes of operation (refer to diagrams)
- Transport supports
- Slings gear for rotary drive

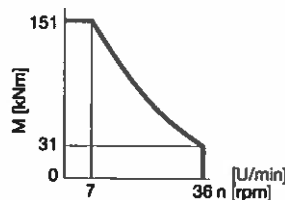
### Optional equipment

- Kelly drive adapter KA 420/368

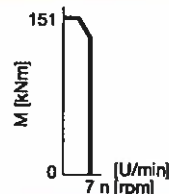
## KDK 150 KL

168 kW Motorleistung  
168 kW engine power

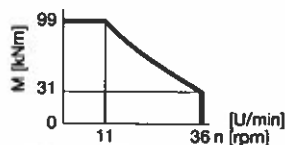
1. Gang Standardbetrieb  
1<sup>st</sup> gear standard mode



1. Gang Einrichten und Felsbohren  
1<sup>st</sup> gear Set up and rock drilling

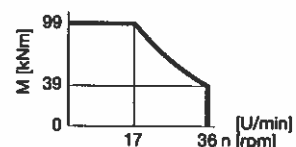
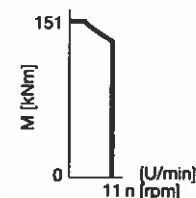
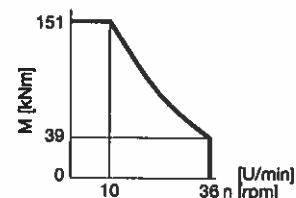


1. Gang M<sub>0</sub> reduziert  
1<sup>st</sup> gear M<sub>0</sub> reduced



## KDK 150 KL

230 kW Motorleistung  
230 kW engine power



Drehmoment nominal, Darstellung nicht maßstäblich  
nominal torque values, not to scale

Das Trägergerät BT 40 wird von Bauer Maschinen geplant und gebaut. Der Motor und das Hydraulikaggregat sind längs eingebaut. Diese Bauweise gewährleistet optimale Luftführung, niedrige Transporthöhe und optimale Kühlleistung bis 40° Außentemperatur.

The base carrier BT 40 is designed and built by Bauer Maschinen. The engine and the hydraulic power pack are mounted in longitudinal direction. Such a construction principle ensures optimal air flow, low transport height, optimal cooling capacity at 40° ambient temperature.



## Motor, Stage III

Nennleistung ISO 3046-1

Motor spezifiziert nach Abgasnorm

## Motor, Stage IV

Nennleistung ISO 3046-1

mit Leistungspaket

Motor spezifiziert nach Abgasnorm

## Engine, Tier 3

Rated output ISO 3046-1

Engine conforms to Exhaust Emission Standard

## Engine, Tier 4 final

Rated output ISO 3046-1

with power package

Engine conforms to Exhaust Emission Standard

## Cummins QSB 6.7

201 kW @ 2100 U/min (rpm)

EEC 97/68EC Stage III und EPA/CARB Tier 3

## Cummins QSB 6.7

201 kW @ 2100 U/min (rpm)

230 kW @ 2100 U/min (rpm)

EEC 97/68EC Stage IV und EPA/CARB Tier 4 final

## Dieseltank

AdBlue Tank (Stage IV)

Schalldruckpegel in Kabine (EN 791, Anh. A)

Schalleistungspegel (2000/14/EG u. EN 791, Anh.A)

## Hydrauliksystem

Hydraulikdruck

Fördermengen (Hauptkreise + Hilfskreis)

Tankinhalt

Unterwagen (Teleskopfahrwerk)

Laufwerksklasse

Spurweite (eingefahren/ausgefahren)

Fahrwerksbreite (eingefahren/ausgefahren)

3-Steg Bodenplatten

Fahrwerkslänge

Zugkraft (effektiv / nominal)

Fahrgeschwindigkeit

Diesel tank

AdBlue tank (Tier 4 final)

Sound pressure level in cabin (EN 791, Annex A)

Sound power level (2000/14/EG u. EN 791, Annex A)

## Hydraulic system

Hydraulic pressure

Flow rates (main circuits + auxiliary circuit)

Hydraulic oil tank capacity

Undercarriage (Retractable crawler frames)

Crawler type

Track width (retracted/extended)

Overall width of crawlers (retracted/extended)

Width of triple grouser track shoes

Overall length of crawlers

Traction force (effective / nominal)

Travel speed

500 l

38 l

L<sub>pk</sub> 80 dB(A)

L<sub>wa</sub> 112 dB(A)

Zweikreisbohrhydraulik  
2-hydraulic circuit system for drilling

300 bar

2 x 180 l/min + 1 x 105 l/min

500 l

UW 45

B 60

2.400 / 3.400 mm

3.000 / 4.000 mm

600 mm

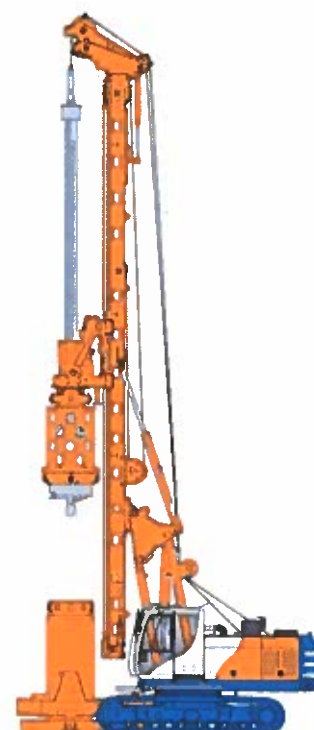
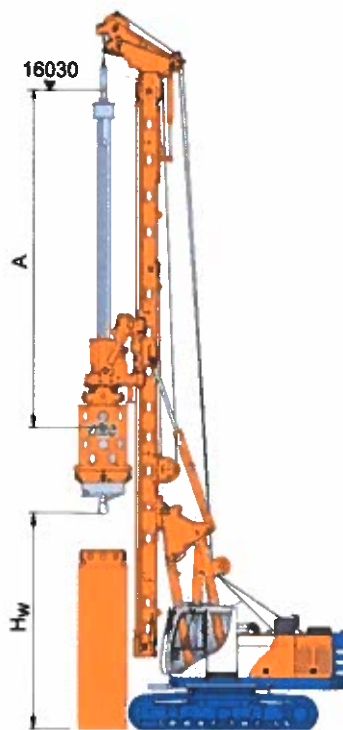
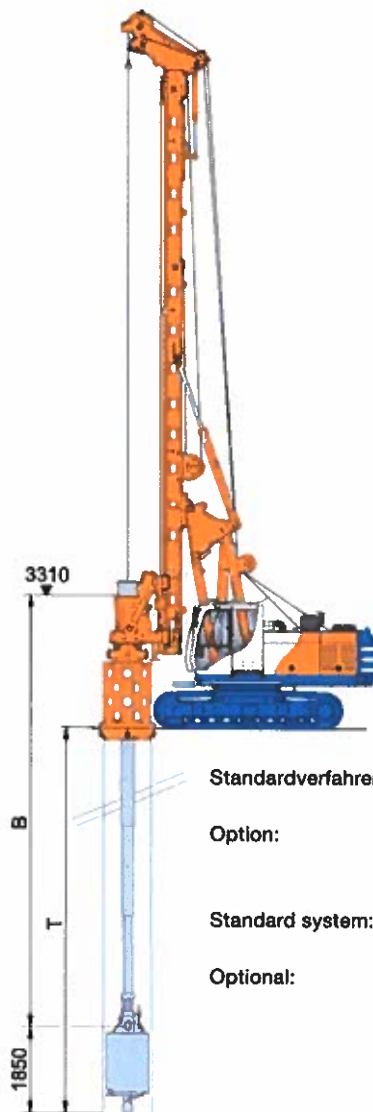
4.710 mm

360 / 430 kN

1,5 km/h

## Kellybohrverfahren

## Kelly drilling system



**Standardverfahren:** unverrohrt, oder Einbau der Verrohrung mit Drehgetriebe

**Option:** Einbau der Verrohrung mit angebauter hydraulischer Verrohrungsmaschine

**Standard system:** Uncased drilling or installation of casing with rotary drive

**Optional:** Installation of casing with hydraulic oscillator attached to the drilling rig

### Zusatzausstattung / optional equipment:

Anbau Verrohrungsmaschine  
Attachment of hydraulic oscillator  
BV 1300 L-03

Bemerkungen zur Bohrdatenermittlung  
siehe „Kellystangen 905.518.1“

For further details on the acquisition of  
drilling data please refer to  
“Kelly Bars 905.518.1”

Bohrtiefen			Drilling depths		
Kellytyp	A (m)	B (m)	Gewicht	Hw (m)	T (m)
Type of kelly bar			Weight (kg)		
BK 15/343/3/18	8,30	20,20	2.930	5,40	18,70
BK 15/343/3/24	10,30	26,20	3.580	3,60	24,70
BK 15/343/3/30	12,30	32,20	4.300	1,60	30,70
BK 15/343/4/24	8,16	26,39	3.840	5,40	24,90
BK 15/343/4/32	10,16	34,39	4.620	3,70	32,90
BK 15/343/4/40	12,16	42,39	5.400	1,70	40,90

Bohrdurchmesser		Drilling diameter
Unverrohrt	Uncased	1.500 mm
Verrohrt	Cased	1.200 mm

Bohrrohrlängen		Length of casing sections
Ohne BV	Without casing oscillator	Hw – 0,5 m
Mit BV	With casing oscillator	Hw – 1,5 m

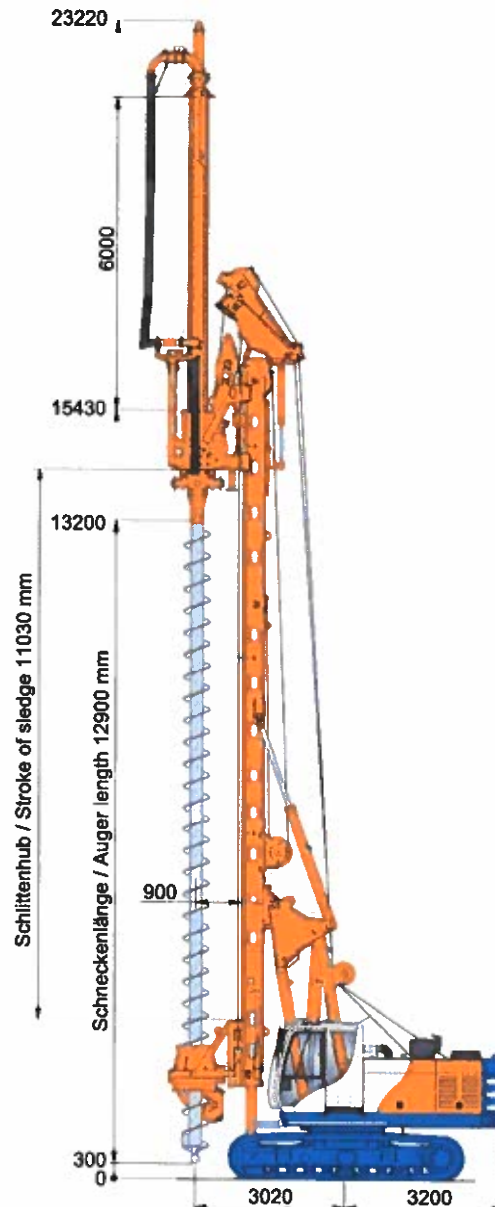
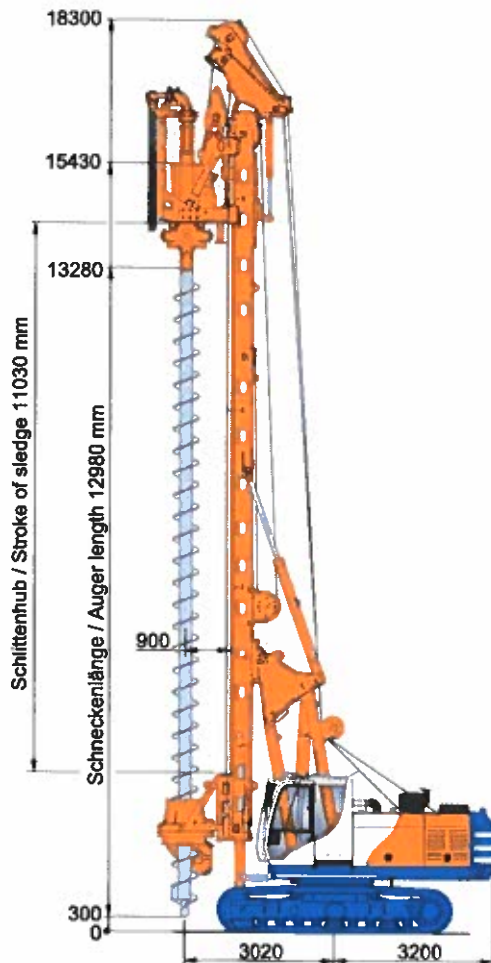


## SOB - Bohrverfahren

## CFA - drilling system

hydraulische Mastabstützung erforderlich  
Hydraulic mast support required

Zeichnung: Kombinierte Zugkraft mit Haupt- und Vorschubwinde mit modifizierter Aufhängung und Traverse  
Drawing: Combined extraction force with crowd winch and main winch with modified connection and spreader beam

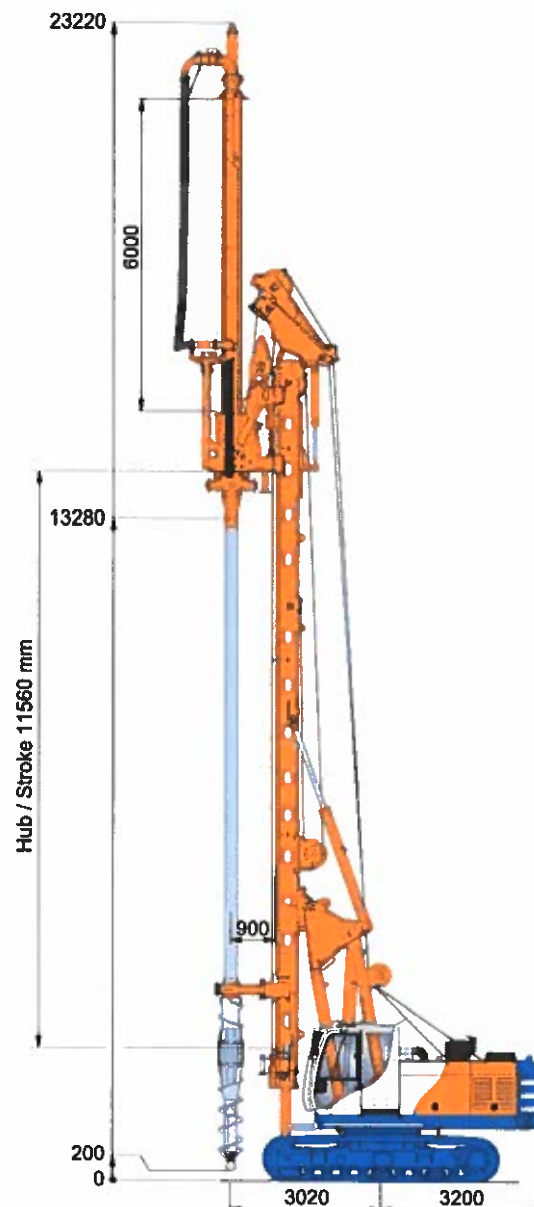
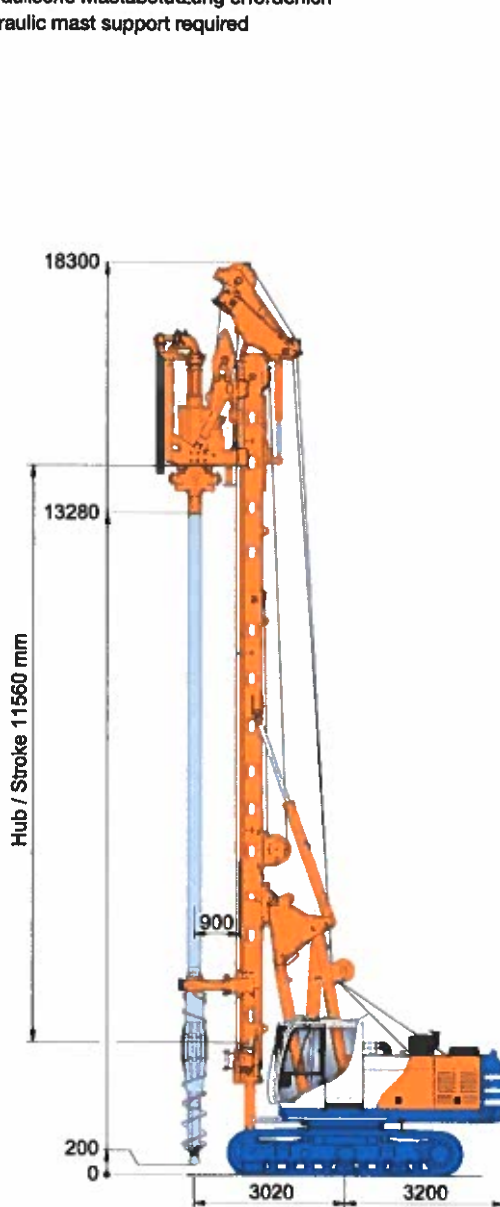


	ohne Kellyverlängerung without Kelly extension	mit Kellyverlängerung 6 m with Kelly extension 6 m
Bohrtiefe mit Schneckenputzer Drilling depth with auger cleaner	10,60 m	16,60 m
Bohrtiefe ohne Schneckenputzer Drilling depth without auger cleaner	11,70 m	17,70 m
Max. Bohrdurchmesser Max. drilling diameter	750 mm	750 mm
Max. Zugkraft Max. extraction force	200 kN	200 kN
Max. Zugkraft mit Haupt- und Vorschubwinde (effektiv) Max. extraction force with main- and crowd winch (effective)	420 kN	420 kN
Max. Anpresskraft Max. crowd force	150 kN + Gewicht Schnecke 150 kN + Weight of auger	150 kN + Gewicht Schnecke 150 kN + Weight of auger

## FDP – Bohrverfahren

## Full displacement piling

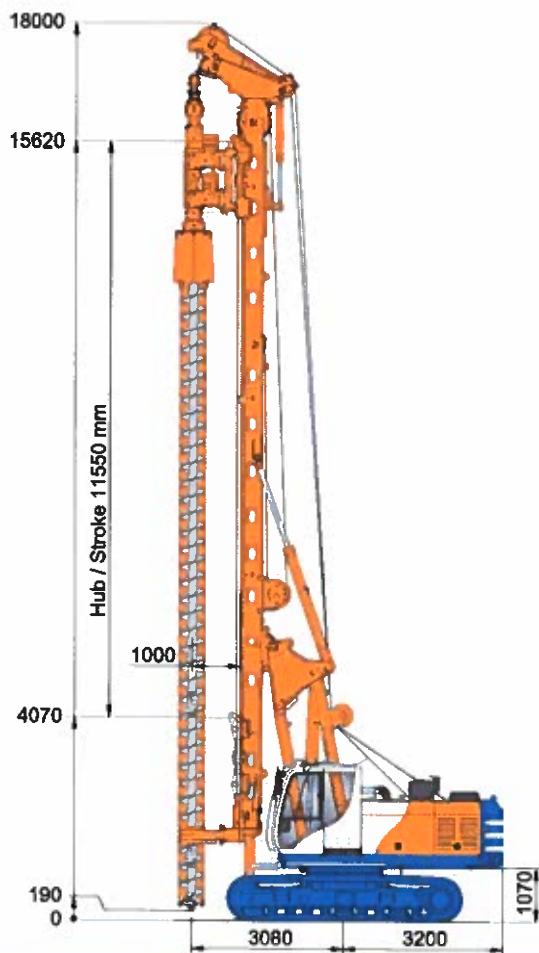
hydraulische Mastabstützung erforderlich  
Hydraulic mast support required



ohne Kellyverlängerung  
without Kelly extension

mit Kellyverlängerung 6 m  
with Kelly extension 6 m

Bohrtiefe Drilling depth	11,20 m	17,20 m
Bohrdurchmesser Drilling diameter	360 – 510 mm	360 – 510 mm
Max. Zugkraft Max. extraction force	200 kN	200 kN
Max. Zugkraft mit Haupt- und Vorschubwinde (effektiv) Max. extraction force with main- and crowd winch (effective)	420 kN	420 kN
Max. Anpresskraft Max. crowd force	150 kN + Verdrängerausrüstung 150 kN + displacement equipment	150 kN + Verdrängerausrüstung 150 kN + displacement equipment



## VdW - Bohrverfahren FoW - drilling system

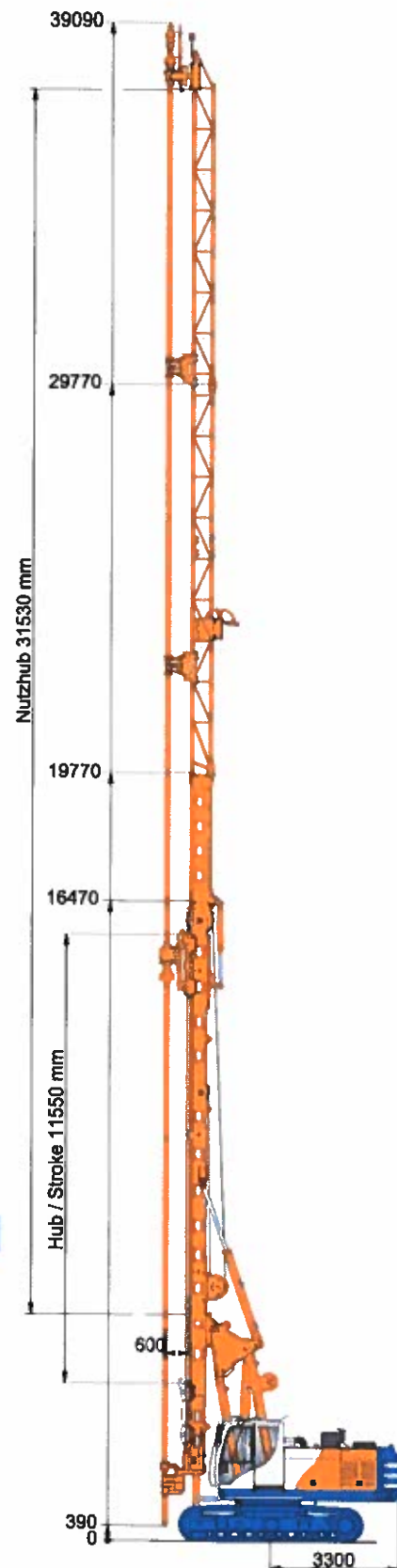
Max. Bohrtiefe	
Max. drilling depth	11,2 m
Bohrdurchmesser	
Drilling diameter	406 – 610 mm
Drehgetriebe	
Rotary drive	DKS 40/60
Leistungspaket 230 kW	empfohlen
Power package 230 kW	recommended

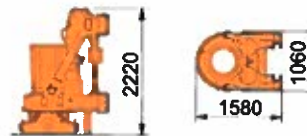
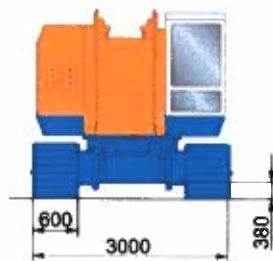
hydraulische Mastabstützung erforderlich  
Hydraulic mast support required

## HDI - Bohrverfahren Jet Grouting - drilling system

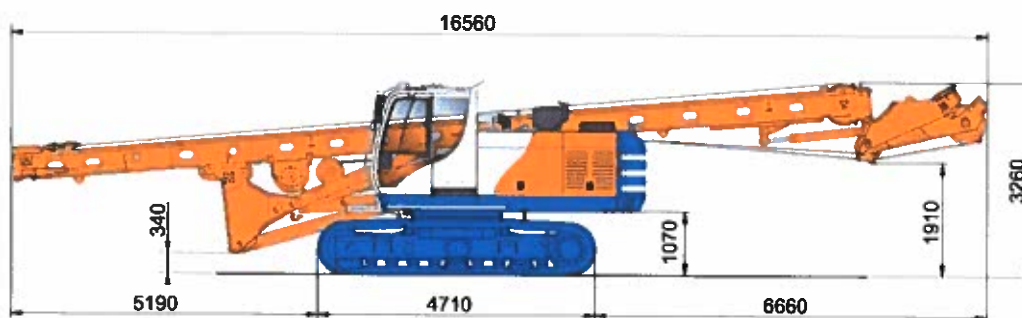
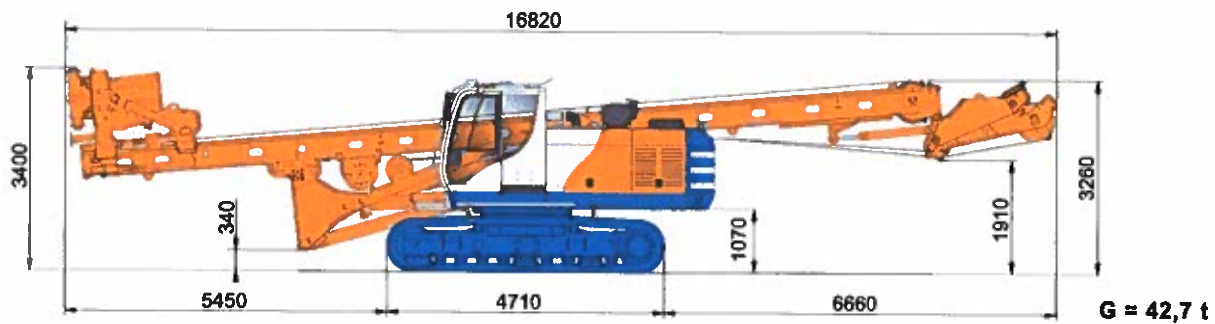
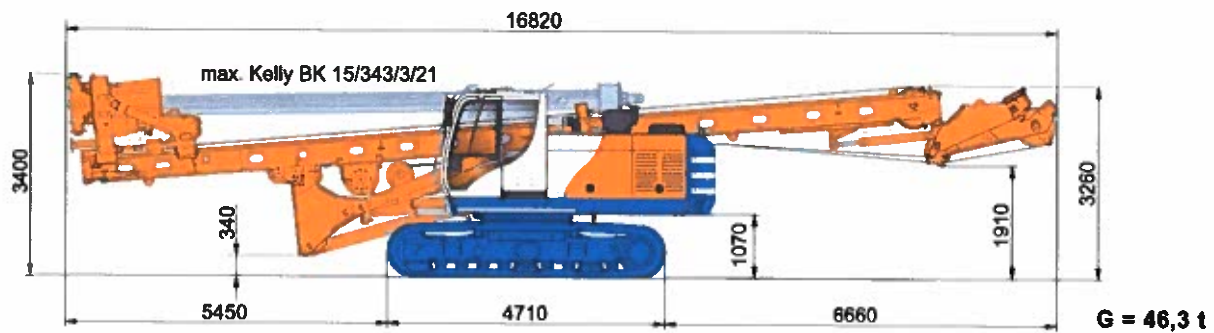
Max. Düstiefe	
Max. jetting depth	30,0 m
Bohrdurchmesser	
Drilling diameter	89 – 133 mm
Drehgetriebe	
Rotary drive	KDK 10 S
Zusatzgegengewicht	
Additional counterweight	2,25 t + 1,0 t

hydraulische Mastabstützung empfohlen  
Hydraulic mast support recommended





**G = 3,7 t**



Gewichtsangaben sind ca. Werte,  
Zusatzausrüstungen (Optionen) können  
das Gesamtgewicht verändern

Weights shown are approximate values,  
optional equipment may change the  
overall weight

**G = 39 t**  
ohne Gegengewicht:  
without counterweight:  
**G = 35 t**



## Die H-Gerätereihe

## The H-model line



**BG 15 H  
BT 40**



**BG 18 H  
BT 50**



**BG 20 H  
BT 60**



**BG 24 H  
BT 75**



**BG 28 H  
BT 85**



**BG 34 H  
BS 95**

*PremiumLine*



bma.bauer.de



**BAUER Maschinen GmbH**  
**BAUER-Straße 1**  
**86529 Schrobenhausen**  
**Germany**  
**Tel. +49 82 52 97-0**  
**bma@bauer.de**  
**www.bauer.de**

Konstruktionsentwicklungen und Prozessverbesserungen können Aktualisierungen und Änderungen von Spezifikation und Materialien ohne vorherige Ankündigung oder Haftung erforderlich machen. Die Abbildungen enthalten möglicherweise optionale Ausstattung und zeigen nicht alle möglichen Konfigurationen. Diese Angaben und die technischen Daten haben ausschließlich Informationscharakter. Irrtum und Druckfehler vorbehalten.

Design developments and process improvements may require the specification and materials to be updated and changed without prior notice or liability. Illustrations may include optional equipment and not show all possible configurations. These and the technical data are provided as indicative information only, with any errors and misprints reserved.



# TOUGHER > FASTER > SIMPLER



## EX90/130

90,000 / 130,000 ft-lb  
122 / 176 kNm

**SPIN OFF** 100 rpm

**LINEPULL**

30,000 / 40,000 lb  
133 / 178 kN

**WEIGHT**

107,000 / 113,000 lbs  
48.5 / 51.2 mT

**MAX DEPTH** 94 ft, 28.7 m

[WATSONUSA.COM](http://WATSONUSA.COM)

800-927-8486



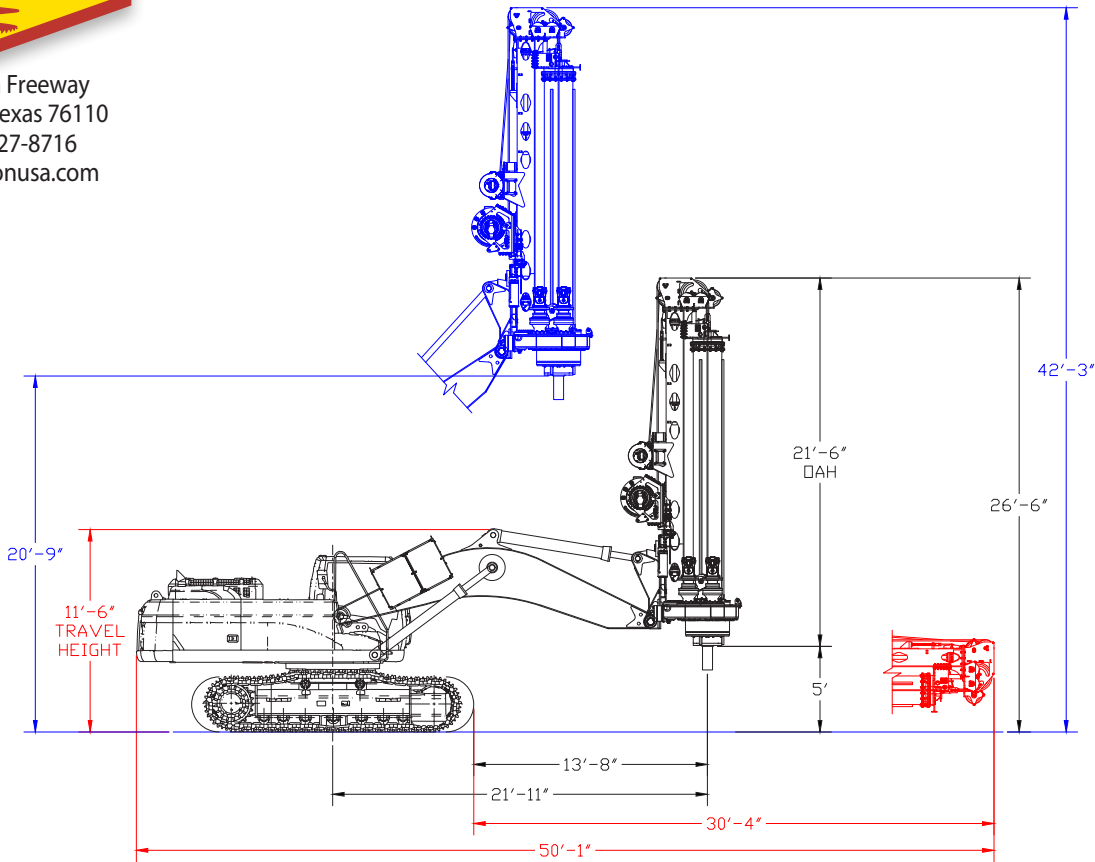
# DRILL MORE HOLES





4015 South Freeway  
Fort Worth, Texas 76110  
Fax 817-927-8716  
sales@watsonusa.com

# EXCADRILL - EX90/130



PERFORMANCE	EX90	EX130
TORQUE	90,000 ft-lb	130,000 ft-lb
	122 kNm	176 kNm
DRILL SPEED	0 TO 60 rpm	
SPIN OFF	100 rpm	100 rpm
KELLY WINCH With FREEFALL	30,000 lbs	40,000 lbs
	133 kN	178 kN
SERVICE WINCH	12,000 lbs	12,000 lbs
	53 kN	53 kN
CROWD FORCE	25,000 lbs	30,000 lbs
	111 kN	133 kN

## CONFIGURATION

BASE MACHINE	CAT 329FL	CAT 336FL
TRANSPORT WEIGHT	107,000 lbs	113,000 lbs
	48,530 kgs	51,255 kgs
DRILLING DEPTH (5-ELEMENT)	94 ft	94 ft
	28.7M	28.7M
SIDE TILT	7° left/right	

## DEFINING FEATURES

- Tri-Drive Rotary** achieves max torque and max spinoff without clutches or gear shifting
- Full excavator horsepower** delivered to the tool
- Interchangeable Heavy Duty Kellys**, swap square & round kellys to match drilling conditions
- Large diameter 24" Rotary** utilizes **bigger bars** which means less wear
- Full Top Crowd** drills straighter holes and simplifies bar locking
- Single layer, grooved Kelly winch** drum for max linepull and longer rope life
- Controlled freefall**, 2-speed Kelly winch for faster cycle times
- Optimized hydraulic interface** for simpler operation and maintenance

## STANDARD OPTIONS

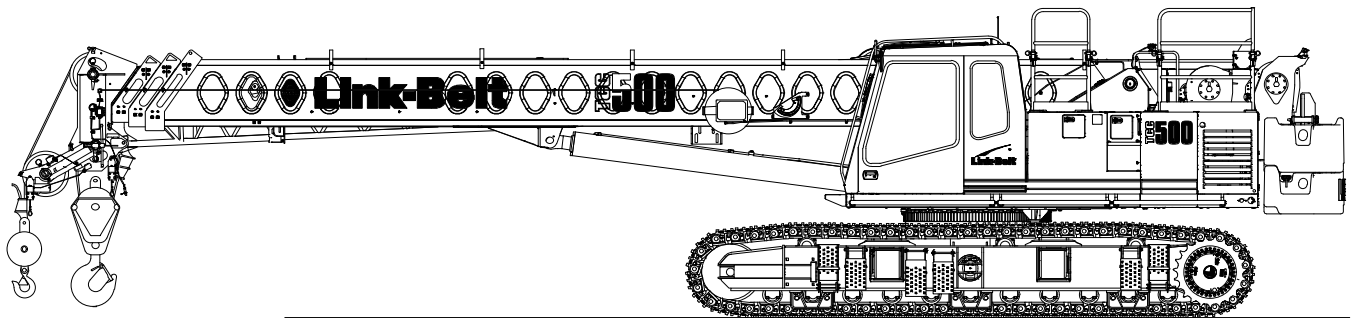
- Custom mast heights and bar sets available** to meet specific drill depth needs
- Can be mounted to any make excavator from 29-45 metric ton**
- Quick disconnect boom/counterweight**
- Customer Kelly stubs/service winches/paint schemes**
- Reaction Jack for increased performance on hard rock**

# Technical Data

## Specifications & Capacities

# TCC500

**Telescopic Crawler Crane**  
50 Ton (51mt Export Machine)



CAUTION: This material is supplied for reference use only. Operator must refer to in-cab Crane Rating Manual and Operator's Manual to determine allowable crane lifting capacities and assembly and operating procedures.

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# Upper Structure

## Frame

All welded steel frame with precision machined surfaces for mating parts.

### Turntable Bearing

- Inner race is bolted to upper frame
- Outer race with external swing gear is bolted to lower frame

## Engine

### Engine

Full pressure lubrication, oil filter, air cleaner, hour meter, throttle, and electric control shutdown.

Specification	Cummins QSB	
	Tier 4f (Stage 3B)	Tier 3 (Stage 3A)
Numbers of Cylinders	6	6
Cycle	4	4
Bore & Stroke: inch (mm)	4.21 x 4.88 (107 x 124)	4.21 x 4.88 (107 x 124)
Piston Dis- placement: in <sup>3</sup> (L)	409 (6.7)	409 (6.7)
Max. Brake Horsepower: hp (kW)	215 (160) @ 1,800 rpm	205 (153) @ 1,800 rpm
Peak Torque: ft lb (Nm)	700 (949) @ 1,500 rpm	689 (929) @ 1,300 rpm
Alternator: volt — amps	12 — 150	12 — 160
Crankcase Capacity: qt (L)	19 (18)	19 (18)
<ul style="list-style-type: none"> <li>• Engine driven variable speed viscus fan clutch and thermostatically controlled radiator</li> </ul>		

### Fuel Tank

One 80 gal (303L) capacity fuel tank.

## Hydraulic System

### Hydraulic Pumps

The pump arrangement is designed to provide hydraulically powered functions allowing positive, precise control with independent or simultaneous operation of all crane functions.

- One variable displacement pumps provide independent control for hoist drums, boom hoist, boom extend, and right & left travel.
- Two gear type pumps are used for the swing, retract cylinders & operator's controls and hydraulic oil cooling fan.

### Hydraulic Reservoir

133 gal (504L) capacity equipped with sight level gauge. Diffusers built in for deaeration.

### Filtration

One 10 micron, full flow return line filter. Accessible for easy filter replacement.

### Counterbalance Valves

All hoist motors are equipped with counterbalance valves to provide positive load lowering and prevent accidental load drop if the hydraulic pressure is suddenly lost.

## Load Hoist Drums

### Main and Optional Auxiliary Winches

- Axial piston, full and half displacement (2-speed) motor driven through planetary reduction unit for positive control under all load conditions.
- Grooved lagging
- Power up/down mode of operation
- Hoist drum cable follower — optional
- Drum rotation indicator
- Drum diameter: 10.63 in (27cm)
- Rope length:
  - Main: 600 ft (182.9m)
  - Auxiliary: 450 ft (137.2m) or 600 ft (182.9m)
- Maximum rope storage: 737 ft (224.6m)
- Terminator style socket and wedge

**Third wrap indicator — optional** — Visually and audibly warns the operator when the wire rope is on the first/bottom layer and when the wire rope is down to the last three wraps

## Swing System

**Motor/Planetary** — Bi-directional hydraulic swing motor mounted to a planetary reducer for 360° continuous smooth swing at 2.0 rpm

**Swing Park Brake** — 360°, electric over hydraulic, (spring applied/hydraulic released) multi-disc brake mounted on the speed reducer. Operated by a switch in the operator's cab.

**Swing Brake** — 360°, foot operated, hydraulic applied disc brake mounted to the speed reducer

**House Lock** — Two—position house lock (boom over front or rear) operated from the operator's cab

## Counterweight

Consists of a five piece design.

- One "A" counterweight, 12,000 lb (5 443kg)
- One "B" counterweight, 13,000 lb (5 897kg)
- Optional one "C" counterweight, 5,000 lb (2 268kg)
- Optional two "A" carbody counterweights, 3,000 lb (1 361kg) each with tool box built in

## Operator's Cab

Fully enclosed modular steel compartment is independently mounted and padded to protect against vibration and noise.

- All tinted/tempered safety glass
- Sliding entry door and front and rear window
- Swing up roof window with windshield wiper
- Door and window locks
- Hot water heater
- Air conditioner
- Sun visor
- Cloth seat
- Circulating fan
- Windshield wipers and washer
- Dry chemical fire extinguisher
- Engine instrumentation panel (tachometer, voltmeter, engine oil pressure, engine water temperature, fuel level, hydraulic oil temperature, hour meter, and service monitor system)
- Mechanical drum rotation indicators for main (rear) and auxiliary (front) hoist drums
- Six way adjustable seat
- Foot throttle
- Joystick controls
- Optional fully adjustable single axis controls
- Bubble type level
- Ergonomic gauge layout
- Controls shut off lever
- AM/FM Radio
- Travel levers & pedals
- Camera (winch & rear view)

## Rated Capacity Limiter System

**Link—Belt Pulse** — The Link—Belt in-house designed, total crane operating system that utilizes the display as a readout and operator interface for the following systems:

- Crane configuration
- Boom length
- Boom head height
- Allowed load and % of allowed load
- Data logging
- Boom angle
- Radius of load
- Actual load

- Operator settable alarms (include):
  - Maximum and minimum boom angles
  - Maximum tip height
  - Maximum boom length
  - Swing left/right positions
  - Operator defined area (imaginary plane)

**Telematics** — Cellular—based data logging and monitoring system that provides:

- Location and operational settings
- Routine maintenance
- Crane and engine monitoring
- Diagnostic and fault codes

## Machinery House

Hinged doors (four on right side) for machinery access.

## Catwalks

Standard on right and left sides. Catwalks fold up and pin for reduced travel width.

## Optional Vandal Guards

Under design

# Lower Structure

## Carbody

### Lower Frame

All welded box construction frame with precision machined surfaces for turntable bearing and rotating joint.

## Side Frames

### Side Frames

All welded, precision machined, steel frames can be hydraulically extended and retracted with a hydraulic cylinder mounted in the lower frame.

- 12 ft 6.88 in (3.83m) extended gauge
- 10 ft 10.62 in (3.31m) intermediate gauge
- 8 ft 9.74 in (2.68m) retracted gauge
- 19 ft 6.19 in (5.95m) overall length
- 31 in 6 in (0.80m) wide track shoes
- Sealed (oil filled) idler and drive planetaries
- Compact travel drives
- Hydraulic self adjusting tracks

### Track Rollers

- Eleven sealed (oil filled) track rollers per side frame
- Heat treated, mounted on anti—friction bearings

### Tracks

Heat treated, self—cleaning grouser shoes and heat treated track pins with dirt seals. 61 track shoes per side.

- Optional flat or “street” pad

### Take Up Idlers

Cast steel, heat treated, self—cleaning, mounted on sealed tapered roller bearings

## Travel and Steering

Each side frame contains a pilot controlled, bi—directional, axial piston motor and a planetary gear reduction unit to provide positive control under all load conditions.

- 2—speed travel
- Individual control provides smooth, precise maneuverability including full counter—rotation.
- Spring applied, hydraulically released multiple wet—disc type brake controlled automatically
- Maximum travel speed is 2 mph (3.2km/h).
- Designed to 40% gradeability

## Tool Boxes

Two heavy duty steel design tool boxes that bolt onto the carbody.

# Boom

## Design

Four section, box type construction of high tensile steel consisting of one base section and three telescoping sections. The vertical side plates have diamond shaped steel impressions for superior strength to weight ratio. The first telescoping section extends independently by means of one double-acting, single stage hydraulic cylinder with integrated holding valves. The second and third telescoping sections extend proportionally by means of one double-acting, single stage cylinder with integrated holding valves and cables.

## Boom

- 35 ft 6 in—110 ft (10.8—33.8m) four section full power boom
- Two mode boom extension: A\*max mode provides superior capacities by extending the first telescoping section to 60 ft 4 in (18.4m). Standard mode synchronizes all the telescoping sections proportionally to 110 ft (33.5m). Controlled from the operator's cab.
- Mechanical boom angle indicator
- Maximum tip height for A—max mode is 67 ft (20.4m) and standard mode is 115 ft 6 in (35.2m).

## Boom Head

- Four 16.5 in (41.9cm) root diameter sealed bearings nylon sheaves to handle up to eight parts of line
- Easily removable wire rope guards
- Rope dead end lugs on each side of the boom head
- Boom head is designed for quick-reeve of the hook block

## Boom Elevation

- One double acting hydraulic cylinder with integral holding valve
- Boom elevation:  $-3^{\circ}$  to  $78^{\circ}$

# Optional Equipment

## Auxiliary Lifting Sheave

- Single 16.5 in (41.9m) root diameter nylon sheave
- Easily removable wire rope guard
- Does not affect erection of the fly or use of the main head sheaves

## Hook Blocks And Balls

- 25 ton (22.3mt) 3 sheave quick-reeve hook block with safety latch
- 40 ton (36.3mt) 4 sheave quick-reeve hook block with safety latch
- 50 ton (44.6mt) 5 sheave quick-reeve hook block with safety latch
- 8.5 ton (7.7mt) swivel and non-swivel hook balls with safety latch

## Fly & Attachments

- 28.5 ft (11.7m) one piece lattice fly, stowable, offsettable to  $2^{\circ}$ ,  $20^{\circ}$ , and  $40^{\circ}$ . Maximum tip height is 143.5 ft (43.74m).
- 28.5—51 ft (8.7—15.6m) two piece bi-fold lattice fly, stowable, offsettable to  $2^{\circ}$ ,  $20^{\circ}$ , and  $40^{\circ}$ . Maximum tip height is 165.5 ft (50.44m).

## Work Platform

- Boom mounted work platform under design.

## Auger Mounting (Under Design)

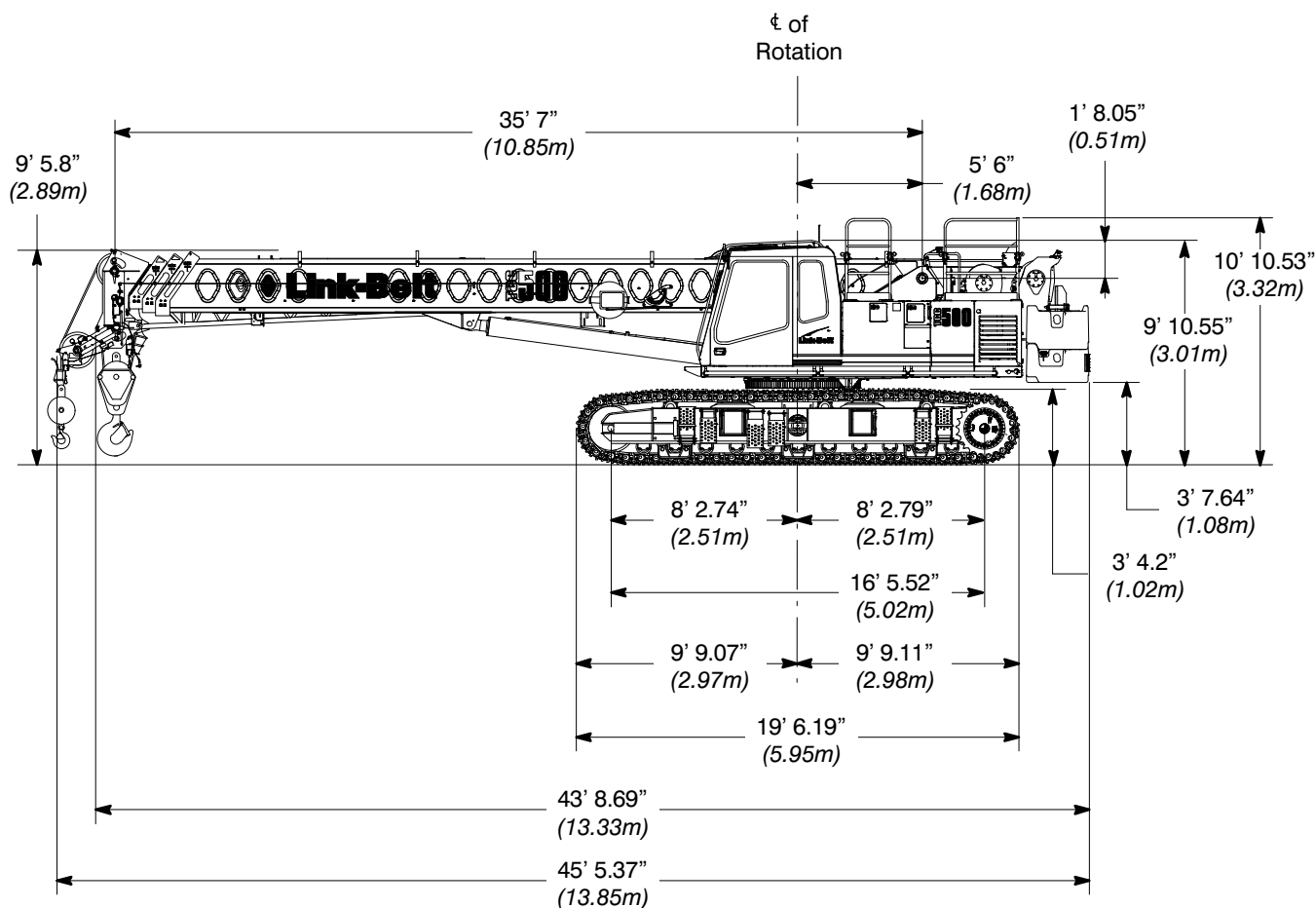
This option provides for all parts required for installation of "Pengo Model DT15 & RT—20 Augers". Included in option are all operator cabin controls, main hydraulic valve, and plumbing. The auger mounts to the boom tip section in operational mode and stores on the base section when not working. Design allows for limited boom extend and retract while drilling, allowing for straight vertical drilling.

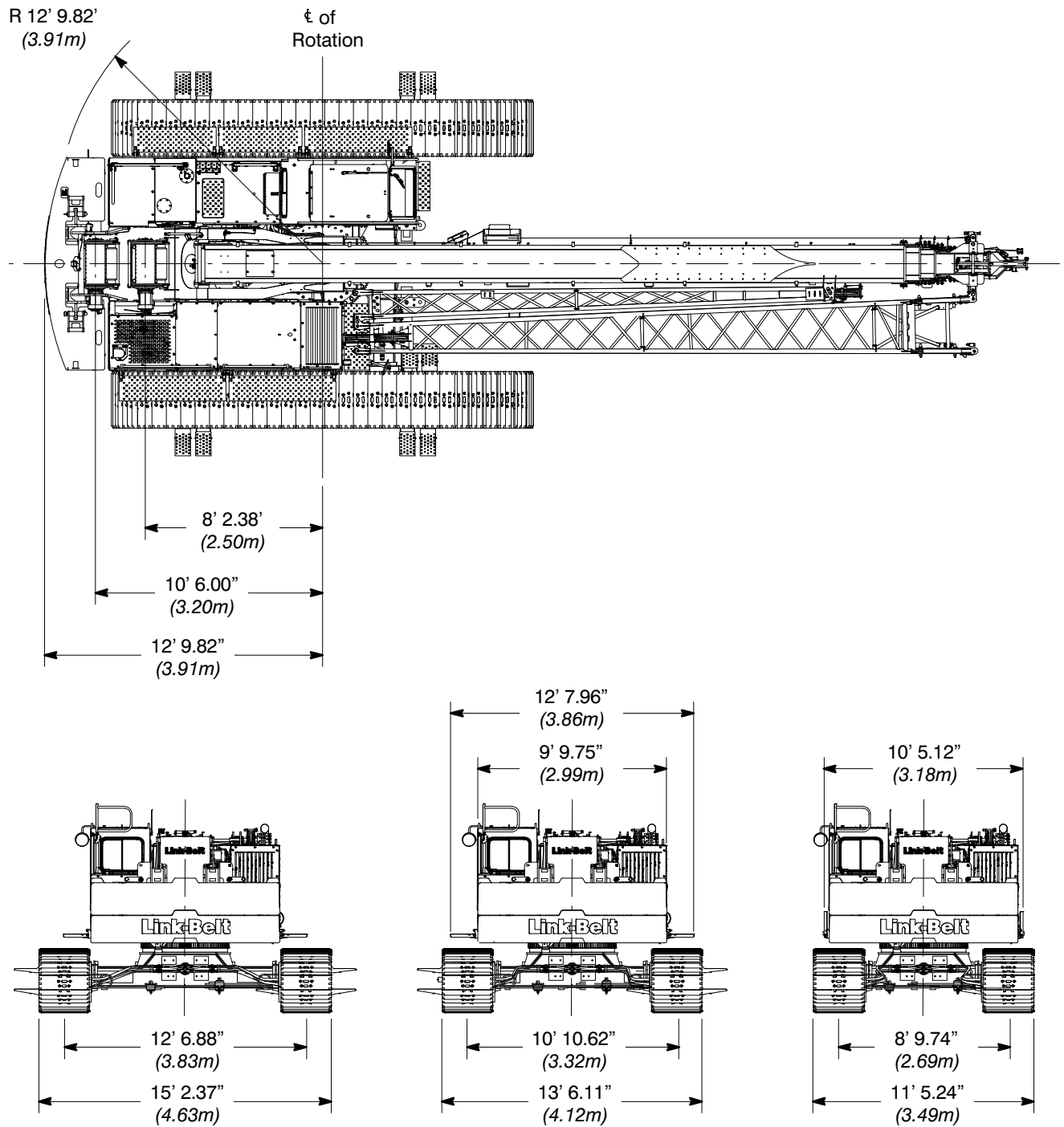


# Dimensions

## Base Crane

General Dimensions	English	Metric
Basic Boom	35.5–110 ft	10.8–33.5m
Minimum Load Radius	10 ft	3.05m
Maximum Boom Angle	78°	78°
Track Shoe Width	31.5 in	0.80m

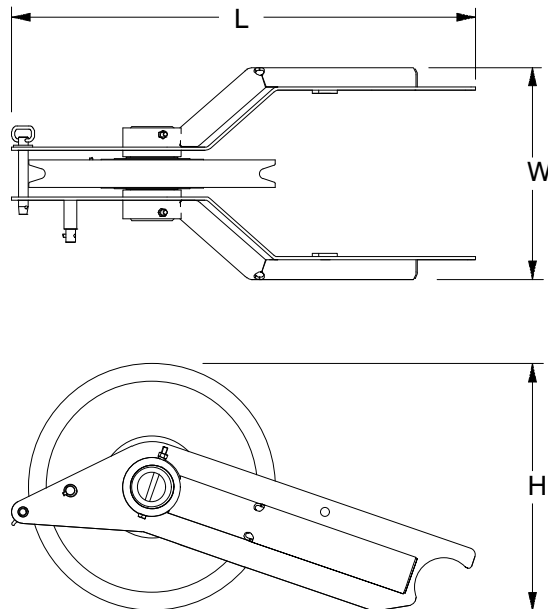




# Auxiliary Lifting Sheave

## Auxiliary Lifting Sheave ①

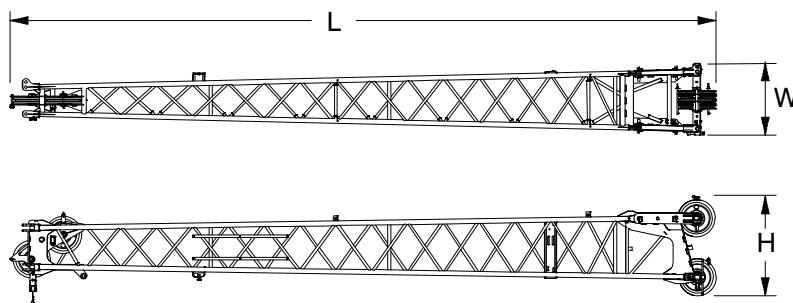
Length	35.31 in	(0.90m)
Width	16.31 in	(0.41m)
Height	19 in	(0.48m)
Weight	92.5 lb	(42kg)



## Fly

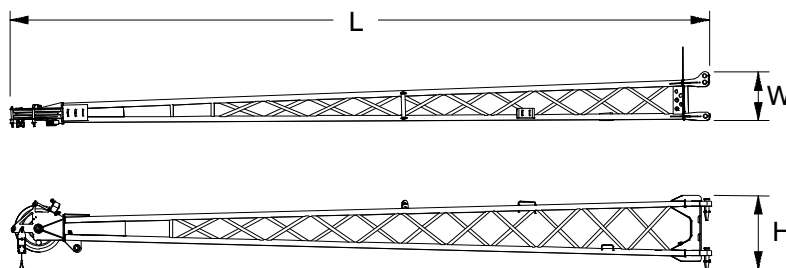
### 28.5 ft (8.69m) Offset Fly One Piece Lattice Fly (Base Fly) ①

Length	28.5 ft	(8.69m)
Width	29 in	(0.74m)
Height	30 in	(0.76m)
Weight	1,188 lb	(539kg)



### 22.5 ft (6.86m) Lattice Fly Tip (Addition To Base Fly For 28.5–51 ft (8.69–15.55m) Bi-fold Fly) ①

Length	22.5 ft	(6.86m)
Width	13.78 in	(0.35m)
Height	20 in	(0.51m)
Weight	654 lb	(297kg)



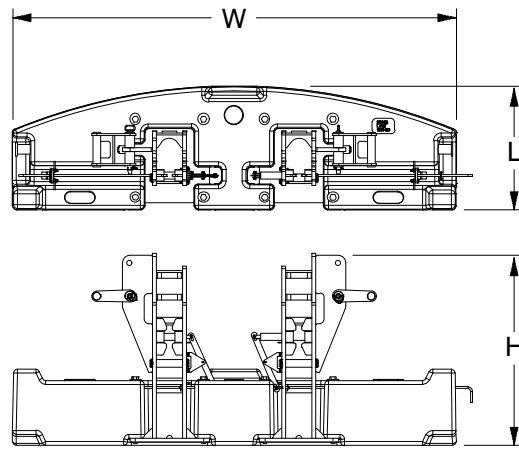
Number inside black circle “①” = # of components

\* — Optional equipment

# Counterweights

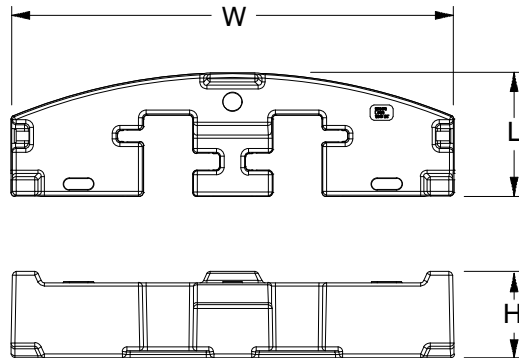
## “A” Counterweight ①

Length	32.90 in	(0.84m)
Width	9 ft 10 in	(3.00m)
Height	4 ft 2.18 in	(1.28m)
Weight	12,000 lb	(5 443kg)



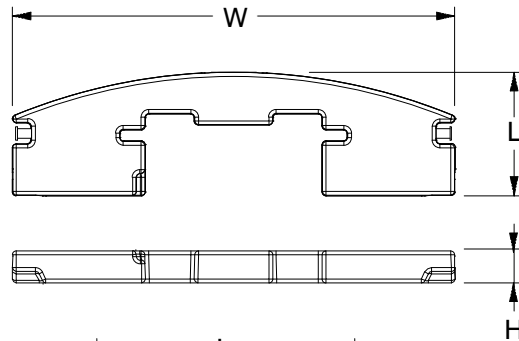
## “B” Counterweights ①

Length	32.90 in	(0.84m)
Width	9 ft 10 in	(3.00m)
Height	23 in	(0.58m)
Weight	13,000 lb	(5 897kg)



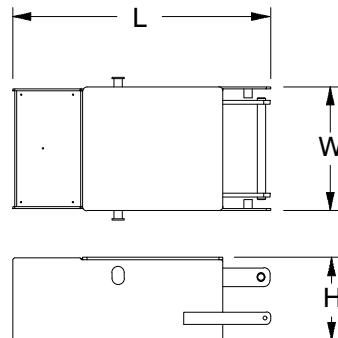
## Optional “C” Counterweights ①

Length	32.90 in	(0.84m)
Width	9 ft 10 in	(3.00m)
Height	8.50 in	(0.22m)
Weight	5,000 lb	(2 268kg)



## Optional “A” Carbody Counterweights ②

Length	62.50 in	(1.59m)
Width	30 in	(0.76m)
Height	20.12 in	(0.51m)
Weight	3,000 lb	(1 361kg)



Number inside black circle “①” = # of components

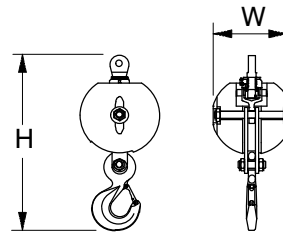
\* — Optional equipment

# Hook Balls

## 8.5 Ton (7.7mt) Swivel

### Hook Ball\* ①

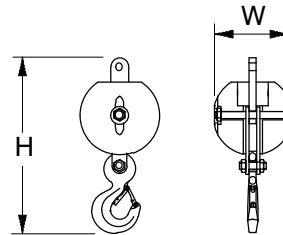
Width	14.50 in	(0.37m)
Height	33.75 in	(0.86m)
Weight	325 lb	(163kg)



## 8.5 Ton (7.7mt) Non—Swivel

### Hook Ball\* ①

Width	14.50 in	(0.37m)
Height	33.80 in	(0.86m)
Weight	360 lb	(163kg)

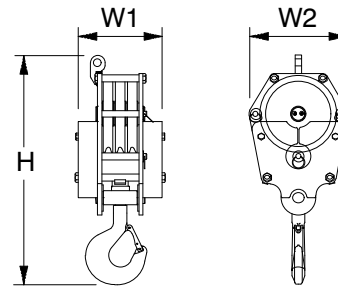


# Hook Blocks

## 25 Ton (22.3mt)

### 3—Sheave Hook Block\* ①

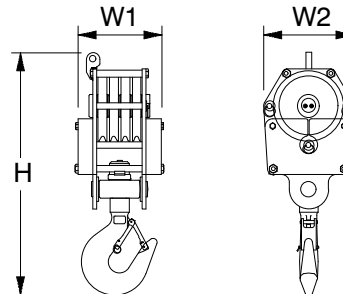
Width1	15.14 in	(0.39m)
Width2	17.88 in	(0.45m)
Height	41.17 in	(1.05m)
Weight	670 lb	(304kg)



## 40 Ton (36.3mt)

### 4—Sheave Hook Block\* ①

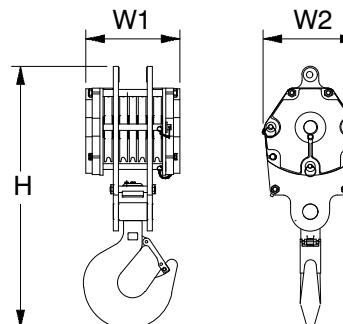
Width1	16.44 in	(0.42m)
Width2	17.88 in	(0.45m)
Height	47.82 in	(1.22m)
Weight	780 lb	(354kg)



## 50 Ton (44.6mt)

### 5—Sheave Hook Block\* ①

Width1	18.75 in	(0.48m)
Width2	18.25 in	(0.46m)
Height	52.31 in	(1.33m)
Weight	1,090 lb	(494kg)



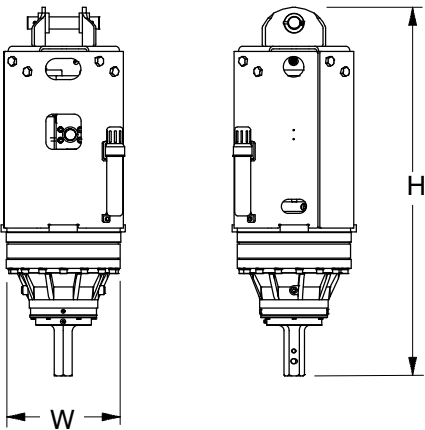
Number inside black circle “①” = # of components

\* — Optional equipment

# Augers

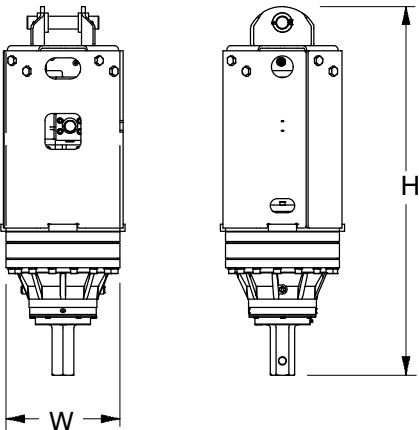
## DT–15 Auger\* ❶

Width	16.12 in	(0.41m)
Height	52.12 in	(1.32m)
Weight	710 lb	(322kg)
Hex Shaft	2.5 in	(6.35cm)



## RT–20 Auger\* ❶

Width	16.12 in	(0.41m)
Height	52.12 in	(1.32m)
Weight	737 lb	(334kg)
Hex Shaft	3 in	(7.62cm)



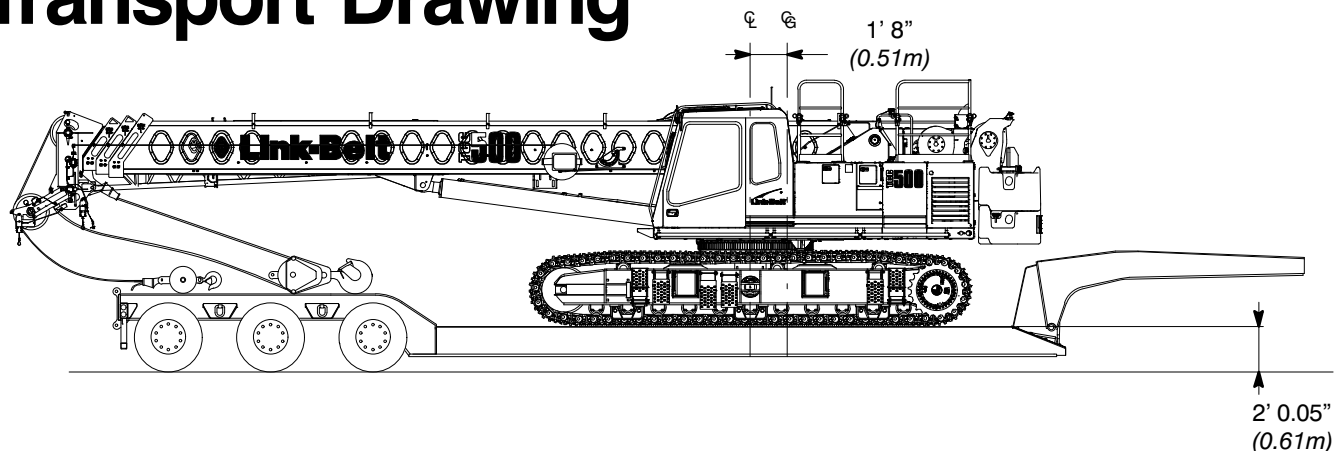
Number inside black circle “❶” = # of components  
\* — Optional equipment

# Working Weights

Option	Description	Gross Weight lb (kg)	Ground Bearing Pressure (on soft ground) psi (kg/cm <sup>2</sup> )
1	Base crane, "AB" counterweight, lower toolbox, 600 ft (182.9m) type "ZB" main wire rope, 450 ft (137.2m) type "ZB" auxiliary wire rope, 2—piece fly, 40 ton (36.29mt) 4 sheave hook block, 8.5 ton (7.71mt) hook ball, and a 250 lb (113kg) operator.	100,000 (45 359kg)	8.88 (0.62)

Notes: Ground bearing pressure is based on the total weight distributed evenly over the track contact area.

## Transport Drawing



**Transport Weight — 99,750 lb (45 246kg)**

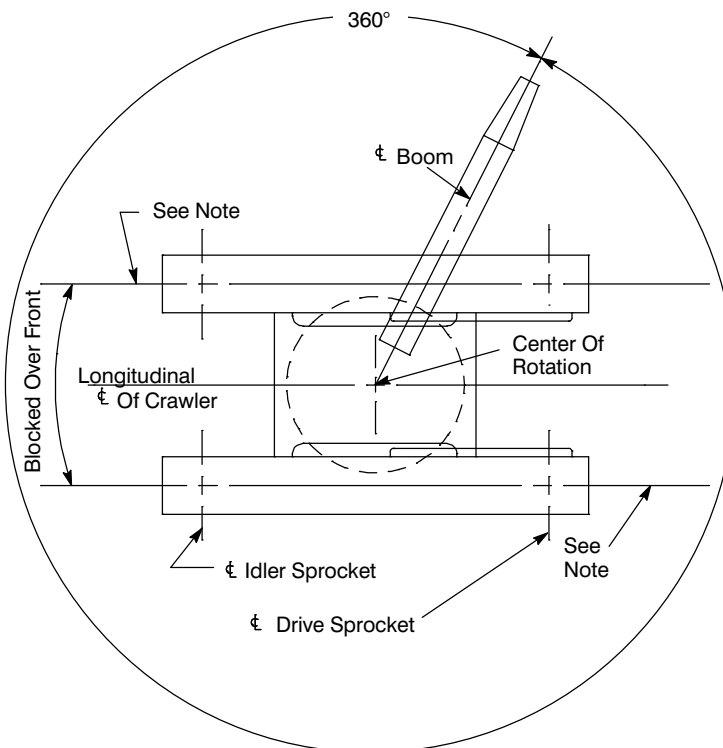
Base crane, "AB" Counterweight, 600 ft (182.9m) type "ZB" main wire rope, 450 ft (137.2m) type "ZB" auxiliary wire rope, 2—piece fly, 40 ton (36.29mt) 4 sheave hook block, and 8.5 ton

## Load Hoist Performance

Main (Rear) and Auxiliary (Front) Winches — 5/8 in (16mm) Rope										
Layer	Maximum Line Pull		Normal Line Speed		High Line Speed		Layer		Total	
	lb	kN	ft/min	m/min	ft/min	m/min	ft	m	ft	m
1	17,084	75.99	181	55.2	360	109.6	97	29.6	97	29.6
2	15,454	68.74	200	61.1	398	121.2	107	32.6	205	62.4
3	14,107	62.75	219	66.9	436	132.8	118	35.9	322	98.3
4	12,977	57.72	239	72.7	474	144.3	128	39.0	451	137.3
5	12,014	53.44	258	78.6	511	155.9	138	42.1	589	179.5
6	11,184	49.75	277	84.4	549	167.5	149	45.3	737	224.7

Wire Rope Application		Diameter		Type	Maximum Permissible Load	
		in	mm		lb	kg
Main (Rear) Winch	Standard	5/8	16	34x7 rotation resistant — right regular lay or right lang lay (Type ZB)	11,080	5 025.8
	Optional	5/8	16	18x19 rotation resistant — right regular lay or right lang lay (Type RB)	9,080	4 118.6
	Optional	5/8	16	6x19 IWRC — right regular lay (Type DB)	11,771	5 339.2
Auxiliary (Front) Winch	Standard	5/8	16	34x7 rotation resistant — right regular lay (Type ZB)	11,080	5 025.8
	Optional	5/8	16	18x19 rotation resistant — right regular lay (Type RB)	9,080	4 118.6
	Optional	5/8	16	6x19 IWRC — right regular lay (Type DB)	11,771	5 339.2

# Working Areas



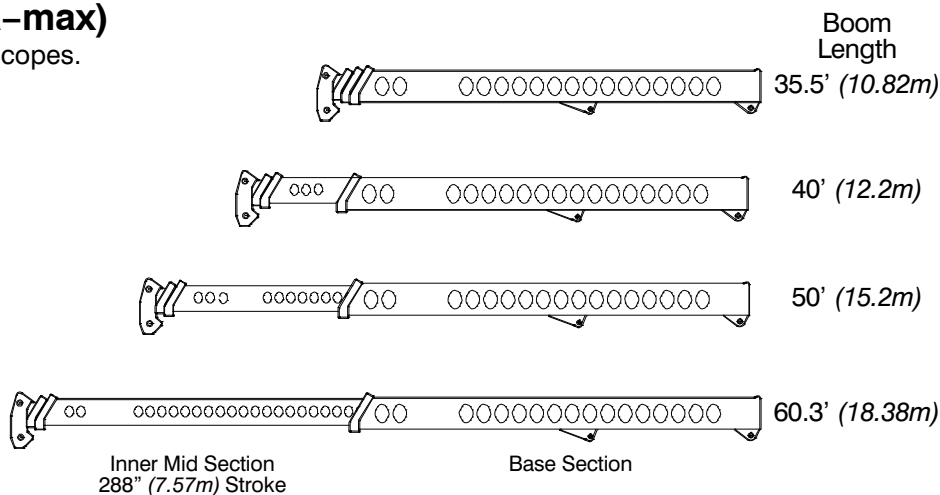
**Note:** These Lines Determine The Limiting Position Of Any Load For Operation Within Working Areas Indicated.



# Boom Extend Modes

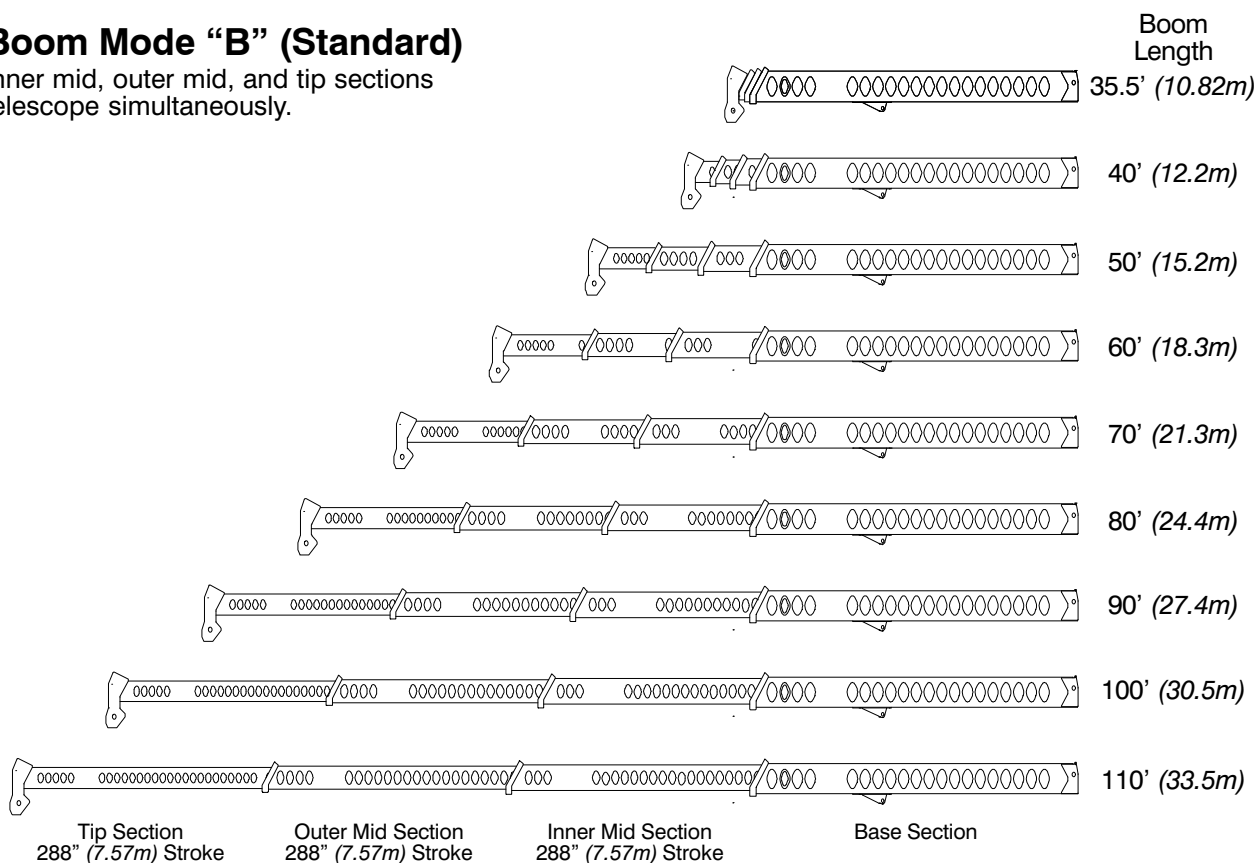
## Boom Mode “A” (A-max)

Only inner mid section telescopes.

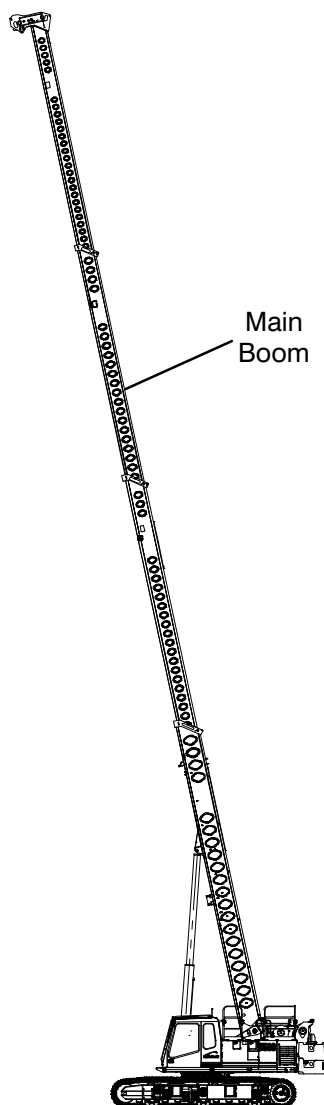


## Boom Mode “B” (Standard)

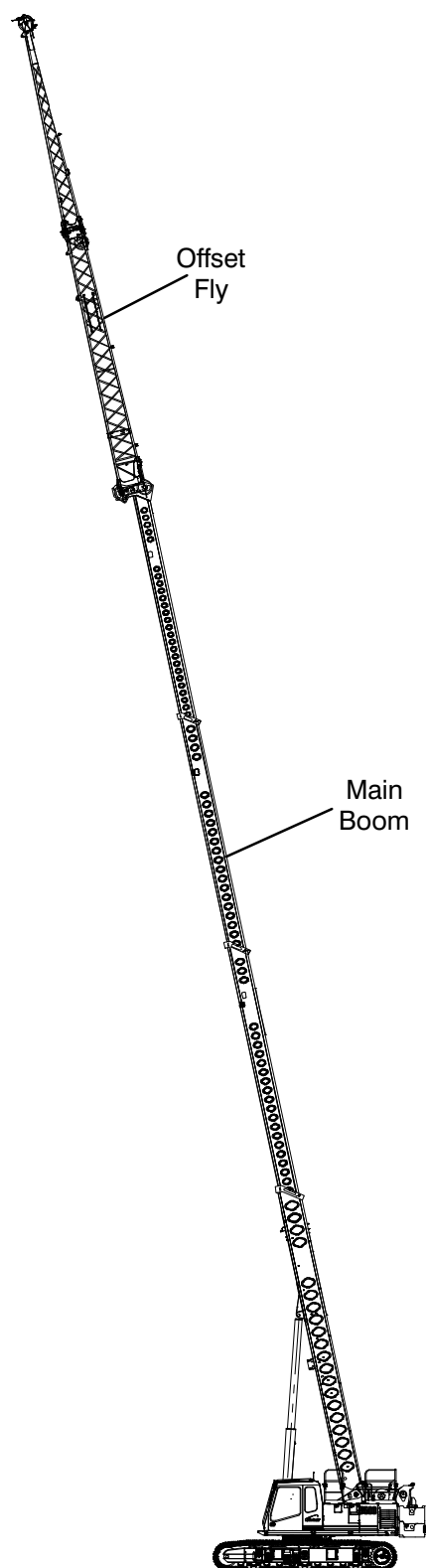
Inner mid, outer mid, and tip sections telescope simultaneously.



# Attachments



**35.5–110 ft (10.82–33.53m)  
Main Boom**



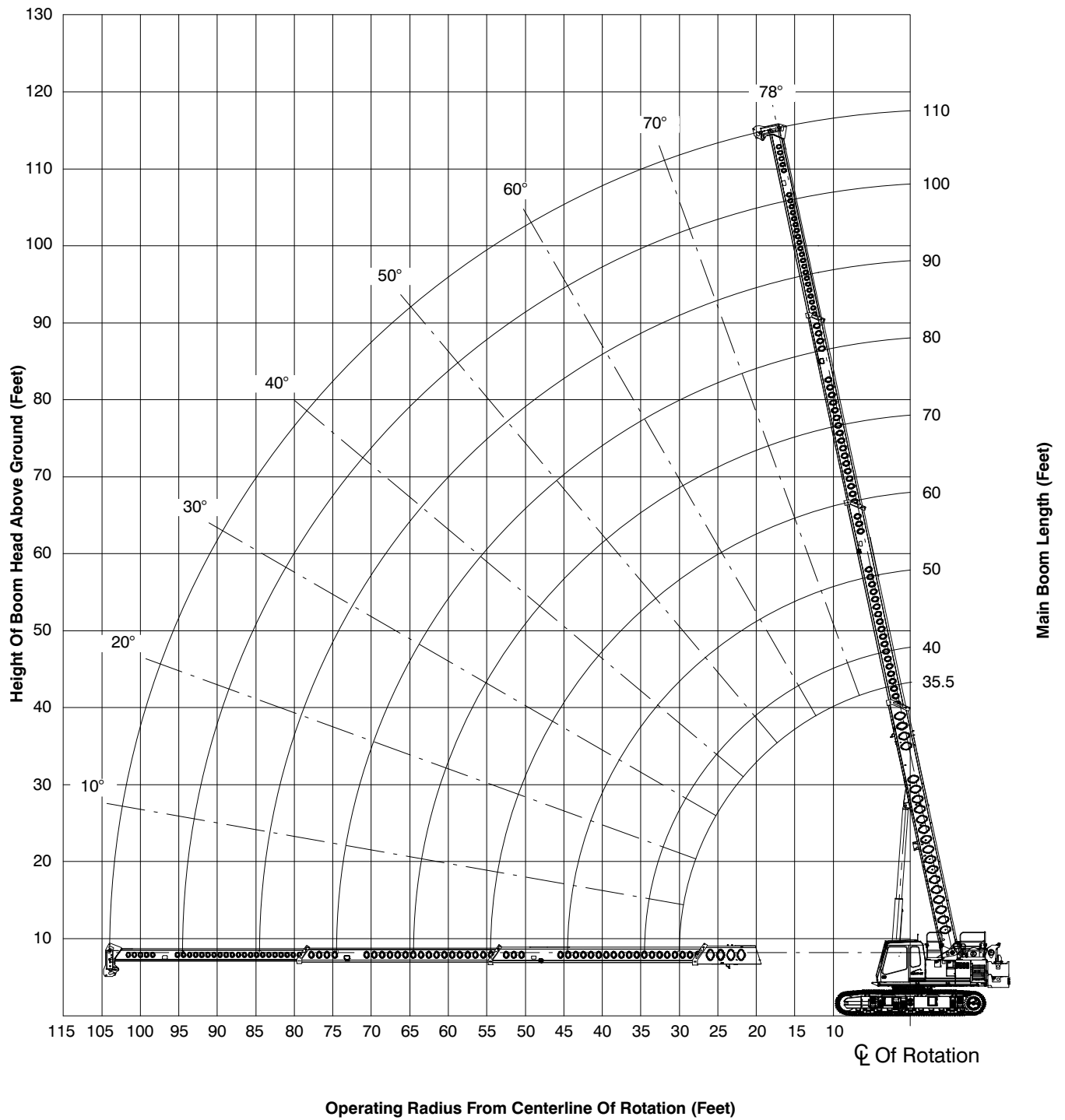
**35.5–110 ft (10.82–33.53m) Main Boom  
With 28.5–51 ft (8.69–15.54m) Offset Fly**

### A—max Mode — Extended Gauge

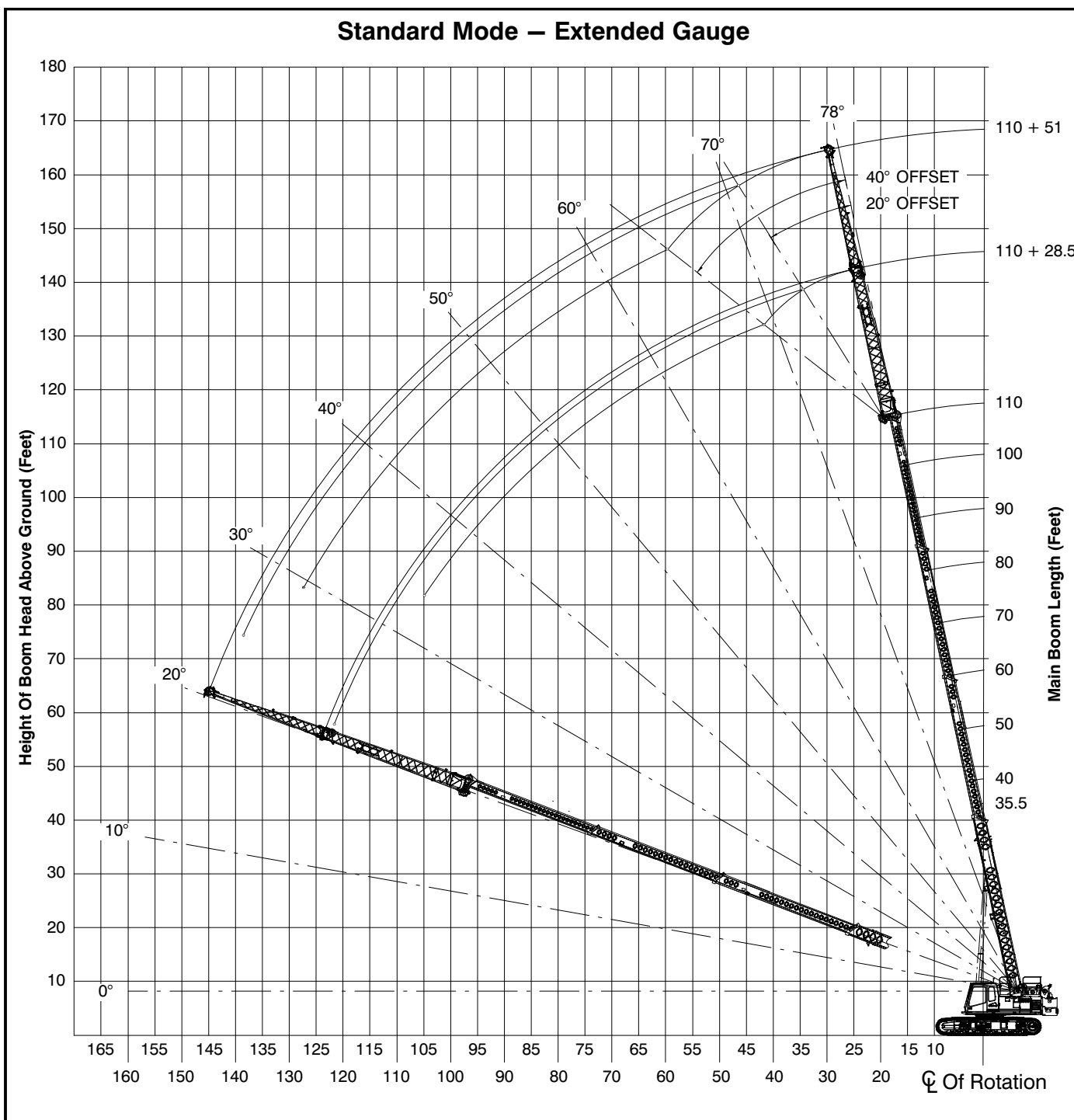
The graph illustrates the relationship between the operating radius and the height of the boom head above ground for different boom lengths. The x-axis represents the Operating Radius From Centerline Of Rotation (Feet), ranging from 65 to 10. The y-axis represents the Height Of Boom Head Above Ground (Feet), ranging from 10 to 80. Four curves are shown for main boom lengths of 35.5, 40, 50, and 60.3 feet. Dashed lines indicate angles from 0° to 78°. An illustration of the crane is provided at the bottom right.

Operating Radius (Feet)	Height (Feet) - 35.5' Boom	Height (Feet) - 40' Boom	Height (Feet) - 50' Boom	Height (Feet) - 60.3' Boom
65	~19	-	-	-
60	~28	-	-	-
55	~38	~18	-	-
50	~48	~28	~18	-
45	~58	~38	~28	~18
40	~68	~48	~38	~28
35	~78	~58	~48	~38
30	~88	~68	~58	~48
25	~98	~78	~68	~58
20	~108	~88	~78	~68
15	~118	~98	~88	~78
10	~128	~108	~98	~88

# Standard — Extended Gauge



# Main Boom + Fly Working Range Diagrams



# Main Boom Load Charts

Main Boom Lift Capacity Chart — 360° Rotation — Side Frames Extended Position AB+0 [25,000 lb (11 340kg)] Counterweight [All capacities are listed in kips (mt)]										
Load Radius ft (m)	Boom Length ft (m)									Load Radius ft (m)
	35.5 (10.8)	40.0 (12.2)	50.0 (15.2)	60.0 (18.3)	70.0 (21.3)	80.0 (24.4)	90.0 (27.4)	100.0 (30.5)	110.0 (33.5)	
10.0 (3.0)	100.0 (45.4)	84.0 (38.1)	82.1 (37.2)							10.0 (3.0)
12.0 (3.7)	88.1 (40.0)	84.0 (38.1)	79.0 (35.8)	53.2 (24.1)	39.0 (17.7)					12.0 (3.7)
15.0 (4.6)	76.8 (34.8)	74.5 (33.8)	69.1 (31.3)	51.1 (23.2)	39.0 (17.7)	40.0 (18.1)				15.0 (4.6)
20.0 (6.1)	47.0 (21.3)	46.8 (21.2)	46.2 (21.0)	42.1 (19.1)	39.0 (17.7)	37.8 (17.1)	31.2 (14.2)			20.0 (6.1)
25.0 (7.6)	32.3 (14.7)	32.7 (14.8)	33.3 (15.1)	33.6 (15.2)	33.7 (15.3)	33.2 (15.1)	27.4 (12.4)	24.7 (11.2)	20.0 (9.1)	25.0 (7.6)
30.0 (9.1)		24.2 (11.0)	24.8 (11.2)	25.2 (11.4)	25.3 (11.5)	25.4 (11.5)	24.2 (11.0)	21.7 (9.8)	19.9 (9.0)	30.0 (9.1)
35.0 (10.7)			19.3 (8.8)	19.7 (8.9)	19.9 (9.0)	20.0 (9.1)	20.1 (9.1)	19.4 (8.8)	17.8 (8.1)	35.0 (10.7)
40.0 (12.2)			15.4 (7.0)	15.8 (7.2)	16.0 (7.3)	16.2 (7.3)	16.3 (7.4)	16.3 (7.4)	16.0 (7.3)	40.0 (12.2)
45.0 (13.7)				12.9 (5.9)	13.2 (6.0)	13.3 (6.0)	13.4 (6.1)	13.5 (6.1)	13.5 (6.1)	45.0 (13.7)
50.0 (15.2)				10.7 (4.9)	11.0 (5.0)	11.2 (5.1)	11.2 (5.1)	11.3 (5.1)	11.3 (5.1)	50.0 (15.2)
55.0 (16.8)					9.2 (4.2)	9.4 (4.3)	9.5 (4.3)	9.6 (4.4)	9.7 (4.4)	55.0 (16.8)
60.0 (18.3)					7.8 (3.5)	8.0 (3.6)	8.1 (3.7)	8.2 (3.7)	8.3 (3.8)	60.0 (18.3)
65.0 (19.8)						6.8 (3.1)	6.9 (3.1)	7.0 (3.2)	7.1 (3.2)	65.0 (19.8)
70.0 (21.3)						5.8 (2.6)	5.9 (2.7)	6.0 (2.7)	6.1 (2.8)	70.0 (21.3)
75.0 (22.9)							5.1 (2.3)	5.2 (2.4)	5.2 (2.4)	75.0 (22.9)
80.0 (24.4)							4.3 (2.0)	4.4 (2.0)	4.5 (2.0)	80.0 (24.4)
85.0 (25.9)								3.8 (1.7)	3.9 (1.8)	85.0 (25.9)
90.0 (27.4)								3.2 (1.5)	3.3 (1.5)	90.0 (27.4)
95.0 (29.0)									2.8 (1.3)	95.0 (29.0)
100.0 (30.5)									2.4 (1.1)	100.0 (30.5)
* 51 metric ton base rating obtained @ 2.5 meters										

This material is supplied for reference use only. Operator must refer to in-cab Crane Rating Manual and Operator's Manual to determine allowable crane lifting capacities and assembly and operating procedures.



<b>Main Boom Lift Capacity Chart — 360° Rotation — Side Frames Intermediate Position</b> <b>ABC+A [36,000 lb (16 329kg)] Counterweight</b> <b>[All capacities are listed in kips (mt)]</b>										
Load Radius ft (m)	Boom Length ft (m)									Load Radius ft (m)
	35.5 (10.8)	40.0 (12.2)	50.0 (15.2)	60.0 (18.3)	70.0 (21.3)	80.0 (24.4)	90.0 (27.4)	100.0 (30.5)	110.0 (33.5)	
10.0 (3.0)	100.0 (45.4)	84.0 (38.1)	82.1 (37.2)							10.0 (3.0)
12.0 (3.7)	88.1 (40.0)	84.0 (38.1)	79.0 (35.8)	53.2 (24.1)	39.0 (17.7)					12.0 (3.7)
15.0 (4.6)	76.8 (34.8)	74.5 (33.8)	69.1 (31.3)	51.1 (23.2)	39.0 (17.7)	40.0 (18.1)				15.0 (4.6)
20.0 (6.1)	54.4 (24.7)	54.2 (24.6)	53.6 (24.3)	42.1 (19.1)	39.0 (17.7)	37.8 (17.1)	31.2 (14.2)			20.0 (6.1)
25.0 (7.6)	37.6 (17.1)	38.1 (17.3)	38.5 (17.5)	38.5 (17.5)	39.0 (17.7)	33.2 (15.1)	27.4 (12.4)	24.7 (11.2)	20.0 (9.1)	25.0 (7.6)
30.0 (9.1)		28.4 (12.9)	29.1 (13.2)	29.4 (13.3)	29.6 (13.4)	29.6 (13.4)	24.2 (11.0)	21.7 (9.8)	19.9 (9.0)	30.0 (9.1)
35.0 (10.7)			22.8 (10.3)	23.1 (10.5)	23.4 (10.6)	23.4 (10.6)	21.4 (9.7)	19.4 (8.8)	17.8 (8.1)	35.0 (10.7)
40.0 (12.2)			18.4 (8.3)	18.8 (8.5)	19.0 (8.6)	19.2 (8.7)	19.2 (8.7)	17.4 (7.9)	16.0 (7.3)	40.0 (12.2)
45.0 (13.7)				15.5 (7.0)	15.8 (7.2)	15.9 (7.2)	16.0 (7.3)	15.7 (7.1)	14.4 (6.5)	45.0 (13.7)
50.0 (15.2)				13.0 (5.9)	13.2 (6.0)	13.4 (6.1)	13.5 (6.1)	13.6 (6.2)	13.1 (5.9)	50.0 (15.2)
55.0 (16.8)					11.3 (5.1)	11.4 (5.2)	11.5 (5.2)	11.6 (5.3)	11.7 (5.3)	55.0 (16.8)
60.0 (18.3)					9.7 (4.4)	9.8 (4.4)	10.0 (4.5)	10.1 (4.6)	10.1 (4.6)	60.0 (18.3)
65.0 (19.8)						8.5 (3.9)	8.6 (3.9)	8.7 (3.9)	8.8 (4.0)	65.0 (19.8)
70.0 (21.3)						7.4 (3.4)	7.5 (3.4)	7.6 (3.4)	7.7 (3.5)	70.0 (21.3)
75.0 (22.9)							6.5 (2.9)	6.6 (3.0)	6.7 (3.0)	75.0 (22.9)
80.0 (24.4)							5.7 (2.6)	5.8 (2.6)	5.9 (2.7)	80.0 (24.4)
85.0 (25.9)								5.1 (2.3)	5.1 (2.3)	85.0 (25.9)
90.0 (27.4)								4.4 (2.0)	4.5 (2.0)	90.0 (27.4)
95.0 (29.0)									3.9 (1.8)	95.0 (29.0)
100.0 (30.5)									3.4 (1.5)	100.0 (30.5)

This material is supplied for reference use only. Operator must refer to in-cab Crane Rating Manual and Operator's Manual to determine allowable crane lifting capacities and assembly and operating procedures.

# Main Boom + Fly Load Charts

<b>90 ft (27.4m) Main Boom + Fly — 360° Rotation — Standard Mode — Side Frames Extended Position</b> <b>AB+0 [25,000 lb (11 340kg)] Counterweight</b> <b>[All capacities are listed in kips (mt)]</b>							
Load Radius ft (m)	28.25 ft Manual Offset Fly			51 ft Manual Offset Fly			Load Radius ft (m)
	2°	20°	40°	2°	20°	40°	
30 (9.1)	16.7 (7.6)						30 (9.1)
35 (10.7)	15.5 (7.0)			9.7 (4.4)			35 (10.7)
40 (12.2)	14.5 (6.6)	10.5 (4.8)		8.6 (3.9)			40 (12.2)
45 (13.7)	13.5 (6.1)	9.9 (4.5)	7.9 (3.6)	8.1 (3.7)			45 (13.7)
50 (15.2)	12.0 (5.4)	9.4 (4.3)	7.6 (3.4)	7.5 (3.4)	5.4 (2.4)		50 (15.2)
55 (16.8)	10.4 (4.7)	8.9 (4.0)	7.4 (3.4)	7.0 (3.2)	5.1 (2.3)		55 (16.8)
60 (18.3)	8.9 (4.0)	8.7 (3.9)	7.2 (3.3)	6.5 (2.9)	4.9 (2.2)		60 (18.3)
65 (19.8)	7.7 (3.5)	8.2 (3.7)	7.0 (3.2)	6.1 (2.8)	4.6 (2.1)	3.7 (1.7)	65 (19.8)
70 (21.3)	6.7 (3.0)	7.2 (3.3)	6.8 (3.1)	5.7 (2.6)	4.4 (2.0)	3.5 (1.6)	70 (21.3)
75 (22.9)	5.9 (2.7)	6.2 (2.8)	6.5 (2.9)	5.4 (2.4)	4.2 (1.9)	3.4 (1.5)	75 (22.9)
80 (24.4)	5.1 (2.3)	5.5 (2.5)	5.7 (2.6)	5.1 (2.3)	4.0 (1.8)	3.3 (1.5)	80 (24.4)
85 (25.9)	4.5 (2.0)	4.8 (2.2)	4.9 (2.2)	4.8 (2.2)	3.9 (1.8)	3.3 (1.5)	85 (25.9)
90 (27.4)	3.9 (1.8)	4.1 (1.9)	4.3 (2.0)	4.4 (2.0)	3.7 (1.7)	3.2 (1.5)	90 (27.4)
95 (29.0)	3.4 (1.5)	3.6 (1.6)	3.7 (1.7)	3.9 (1.8)	3.6 (1.6)	3.1 (1.4)	95 (29.0)
100 (30.5)	2.9 (1.3)	3.1 (1.4)		3.4 (1.5)	3.5 (1.6)	3.1 (1.4)	100 (30.5)
105 (32.0)	2.5 (1.1)	2.6 (1.2)		3.0 (1.4)	3.4 (1.5)	3.1 (1.4)	105 (32.0)
110 (33.5)	2.2 (1.0)			2.7 (1.2)	3.0 (1.4)	3.0 (1.4)	110 (33.5)
115 (35.1)				2.3 (1.0)	2.6 (1.2)	2.7 (1.2)	115 (35.1)
120 (36.6)				2.0 (0.9)	2.2 (1.0)		120 (36.6)
125 (38.1)				1.8 (0.8)	1.9 (0.9)		125 (38.1)
130 (39.6)				1.5 (0.7)	1.6 (0.7)		130 (39.6)
135 (41.1)				1.3 (0.6)			135 (41.1)

This material is supplied for reference use only. Operator must refer to in—cab Crane Rating Manual and Operator's Manual to determine allowable crane lifting capacities and assembly and operating procedures.

**110 ft (33.5m) Main Boom + Fly — 360° Rotation — Standard Mode — Side Frames Extended Position**  
**AB+0 [25,000 lb (11 340kg)] Counterweight**  
**[All capacities are listed in kips (mt)]**

Load Radius ft (m)	28.25 ft Manual Offset Fly			51 ft Manual Offset Fly			Load Radius ft (m)
	2°	20°	40°	2°	20°	40°	
35 (10.7)	11.5 (5.2)						35 (10.7)
40 (12.2)	11.5 (5.2)						40 (12.2)
45 (13.7)	10.9 (4.9)	9.8 (4.4)		6.6 (3.0)			45 (13.7)
50 (15.2)	10.0 (4.5)	9.0 (4.1)	7.5 (3.4)	6.6 (3.0)			50 (15.2)
55 (16.8)	9.2 (4.2)	8.4 (3.8)	7.4 (3.4)	6.6 (3.0)			55 (16.8)
60 (18.3)	8.5 (3.9)	7.8 (3.5)	7.2 (3.3)	6.4 (2.9)	4.9 (2.2)		60 (18.3)
65 (19.8)	7.6 (3.4)	7.3 (3.3)	6.9 (3.1)	6.1 (2.8)	4.7 (2.1)		65 (19.8)
70 (21.3)	6.6 (3.0)	6.8 (3.1)	6.5 (2.9)	5.6 (2.5)	4.5 (2.0)		70 (21.3)
75 (22.9)	5.7 (2.6)	6.1 (2.8)	6.1 (2.8)	5.3 (2.4)	4.3 (2.0)	3.5 (1.6)	75 (22.9)
80 (24.4)	5.0 (2.3)	5.4 (2.4)	5.7 (2.6)	4.9 (2.2)	4.1 (1.9)	3.4 (1.5)	80 (24.4)
85 (25.9)	4.3 (2.0)	4.7 (2.1)	4.9 (2.2)	4.6 (2.1)	4.0 (1.8)	3.3 (1.5)	85 (25.9)
90 (27.4)	3.8 (1.7)	4.1 (1.9)	4.3 (2.0)	4.2 (1.9)	3.9 (1.8)	3.2 (1.5)	90 (27.4)
95 (29.0)	3.3 (1.5)	3.5 (1.6)	3.7 (1.7)	3.7 (1.7)	3.7 (1.7)	3.2 (1.5)	95 (29.0)
100 (30.5)	2.8 (1.3)	3.0 (1.4)	3.2 (1.5)	3.2 (1.5)	3.6 (1.6)	3.1 (1.4)	100 (30.5)
105 (32.0)	2.4 (1.1)	2.6 (1.2)	2.7 (1.2)	2.8 (1.3)	3.2 (1.5)	3.1 (1.4)	105 (32.0)
110 (33.5)	2.0 (0.9)	2.2 (1.0)	2.3 (1.0)	2.4 (1.1)	2.8 (1.3)	3.0 (1.4)	110 (33.5)
115 (35.1)	1.7 (0.8)	1.8 (0.8)		2.1 (1.0)	2.5 (1.1)	2.7 (1.2)	115 (35.1)
120 (36.6)	1.4 (0.6)	1.5 (0.7)		1.8 (0.8)	2.1 (1.0)	2.3 (1.0)	120 (36.6)
125 (38.1)	1.1 (0.5)	1.2 (0.5)		1.5 (0.7)	1.8 (0.8)	2.0 (0.9)	125 (38.1)
130 (39.6)				1.3 (0.6)	1.5 (0.7)	1.6 (0.7)	130 (39.6)
135 (41.1)				1.0 (0.5)	1.2 (0.5)	1.3 (0.6)	135 (41.1)

This material is supplied for reference use only. Operator must refer to in—cab Crane Rating Manual and Operator's Manual to determine allowable crane lifting capacities and assembly and operating procedures.

<b>90 ft (27.4m) Main Boom + Fly — 360° Rotation — Standard Mode — Side Frames Extended Position</b> <b>ABC+A [36,000 lb (16 329kg)] Counterweight</b> <b>[All capacities are listed in kips (mt)]</b>							
Load Radius ft (m)	28.25 ft Manual Offset Fly			51 ft Manual Offset Fly			Load Radius ft (m)
	2°	20°	40°	2°	20°	40°	
30 (9.1)	16.7 (7.6)						30 (9.1)
35 (10.7)	15.5 (7.0)			9.7 (4.4)			35 (10.7)
40 (12.2)	14.5 (6.6)	10.5 (4.8)		8.6 (3.9)			40 (12.2)
45 (13.7)	13.5 (6.1)	9.9 (4.5)	7.9 (3.6)	8.1 (3.7)			45 (13.7)
50 (15.2)	12.4 (5.6)	9.4 (4.3)	7.6 (3.4)	7.5 (3.4)	5.4 (2.4)		50 (15.2)
55 (16.8)	11.4 (5.2)	8.9 (4.0)	7.4 (3.4)	7.0 (3.2)	5.1 (2.3)		55 (16.8)
60 (18.3)	10.5 (4.8)	8.7 (3.9)	7.2 (3.3)	6.5 (2.9)	4.9 (2.2)		60 (18.3)
65 (19.8)	9.4 (4.3)	8.3 (3.8)	7.0 (3.2)	6.1 (2.8)	4.6 (2.1)	3.7 (1.7)	65 (19.8)
70 (21.3)	8.3 (3.8)	8.0 (3.6)	6.8 (3.1)	5.7 (2.6)	4.4 (2.0)	3.5 (1.6)	70 (21.3)
75 (22.9)	7.3 (3.3)	7.7 (3.5)	6.7 (3.0)	5.4 (2.4)	4.2 (1.9)	3.4 (1.5)	75 (22.9)
80 (24.4)	6.5 (2.9)	6.8 (3.1)	6.6 (3.0)	5.1 (2.3)	4.0 (1.8)	3.3 (1.5)	80 (24.4)
85 (25.9)	5.7 (2.6)	6.0 (2.7)	6.2 (2.8)	4.8 (2.2)	3.9 (1.8)	3.3 (1.5)	85 (25.9)
90 (27.4)	5.1 (2.3)	5.3 (2.4)	5.5 (2.5)	4.5 (2.0)	3.7 (1.7)	3.2 (1.5)	90 (27.4)
95 (29.0)	4.5 (2.0)	4.7 (2.1)	4.8 (2.2)	4.3 (2.0)	3.6 (1.6)	3.1 (1.4)	95 (29.0)
100 (30.5)	4.0 (1.8)	4.2 (1.9)		4.1 (1.9)	3.5 (1.6)	3.1 (1.4)	100 (30.5)
105 (32.0)	3.5 (1.6)	3.7 (1.7)		3.9 (1.8)	3.4 (1.5)	3.1 (1.4)	105 (32.0)
110 (33.5)	3.1 (1.4)			3.6 (1.6)	3.3 (1.5)	3.0 (1.4)	110 (33.5)
115 (35.1)				3.3 (1.5)	3.2 (1.5)	3.0 (1.4)	115 (35.1)
120 (36.6)				2.9 (1.3)	3.1 (1.4)	3.0 (1.4)	120 (36.6)
125 (38.1)				2.6 (1.2)	2.8 (1.3)		125 (38.1)
130 (39.6)				2.3 (1.0)	2.4 (1.1)		130 (39.6)
135 (41.1)				2.0 (0.9)			135 (41.1)

This material is supplied for reference use only. Operator must refer to in-cab Crane Rating Manual and Operator's Manual to determine allowable crane lifting capacities and assembly and operating procedures.

**110 ft (33.5m) Main Boom + Fly — 360° Rotation — Standard Mode — Side Frames Extended Position**  
**ABC+A [36,000 lb (16 329kg)] Counterweight**  
**[All capacities are listed in kips (mt)]**

Load Radius ft (m)	28.25 ft Manual Offset Fly			51 ft Manual Offset Fly			Load Radius ft (m)
	2°	20°	40°	2°	20°	40°	
35 (10.7)	11.5 (5.2)						35 (10.7)
40 (12.2)	11.5 (5.2)						40 (12.2)
45 (13.7)	10.9 (4.9)	9.8 (4.4)		6.6 (3.0)			45 (13.7)
50 (15.2)	10.0 (4.5)	9.0 (4.1)	7.5 (3.4)	6.6 (3.0)			50 (15.2)
55 (16.8)	9.2 (4.2)	8.4 (3.8)	7.4 (3.4)	6.6 (3.0)			55 (16.8)
60 (18.3)	8.5 (3.9)	7.8 (3.5)	7.2 (3.3)	6.4 (2.9)	4.9 (2.2)		60 (18.3)
65 (19.8)	7.8 (3.5)	7.3 (3.3)	6.9 (3.1)	6.1 (2.8)	4.7 (2.1)		65 (19.8)
70 (21.3)	7.3 (3.3)	6.8 (3.1)	6.5 (2.9)	5.6 (2.5)	4.5 (2.0)		70 (21.3)
75 (22.9)	6.8 (3.1)	6.4 (2.9)	6.1 (2.8)	5.3 (2.4)	4.3 (2.0)	3.5 (1.6)	75 (22.9)
80 (24.4)	6.3 (2.9)	6.0 (2.7)	5.8 (2.6)	4.9 (2.2)	4.1 (1.9)	3.4 (1.5)	80 (24.4)
85 (25.9)	5.6 (2.5)	5.7 (2.6)	5.5 (2.5)	4.6 (2.1)	4.0 (1.8)	3.3 (1.5)	85 (25.9)
90 (27.4)	4.9 (2.2)	5.3 (2.4)	5.2 (2.4)	4.3 (2.0)	3.9 (1.8)	3.2 (1.5)	90 (27.4)
95 (29.0)	4.4 (2.0)	4.7 (2.1)	4.8 (2.2)	4.1 (1.9)	3.7 (1.7)	3.2 (1.5)	95 (29.0)
100 (30.5)	3.9 (1.8)	4.1 (1.9)	4.3 (2.0)	3.8 (1.7)	3.6 (1.6)	3.1 (1.4)	100 (30.5)
105 (32.0)	3.4 (1.5)	3.6 (1.6)	3.7 (1.7)	3.5 (1.6)	3.4 (1.5)	3.1 (1.4)	105 (32.0)
110 (33.5)	3.0 (1.4)	3.2 (1.5)	3.2 (1.5)	3.2 (1.5)	3.2 (1.5)	3.0 (1.4)	110 (33.5)
115 (35.1)	2.6 (1.2)	2.8 (1.3)		2.9 (1.3)	3.0 (1.4)	2.9 (1.3)	115 (35.1)
120 (36.6)	2.3 (1.0)	2.4 (1.1)		2.6 (1.2)	2.8 (1.3)	2.8 (1.3)	120 (36.6)
125 (38.1)	2.0 (0.9)	2.0 (0.9)		2.3 (1.0)	2.5 (1.1)	2.6 (1.2)	125 (38.1)
130 (39.6)				2.1 (1.0)	2.3 (1.0)	2.4 (1.1)	130 (39.6)
135 (41.1)				1.8 (0.8)	2.0 (0.9)	2.1 (1.0)	135 (41.1)

This material is supplied for reference use only. Operator must refer to in—cab Crane Rating Manual and Operator's Manual to determine allowable crane lifting capacities and assembly and operating procedures.



**TAB 4**





## **PACO VENTURES, LLC**

2296 Meyers Ave., Escondido, CA 92029 (760) 748-6653  
Mike Hagy Mobile - (805) 746-6965

### **Michael Hagy - Lead Foundation Slurry Engineering Consultant ADSC/DFI Member**

Mike has operated as a professional slurry consultant on the West Coast for almost 30 years designing calculated site specific slurry programs and has consulted on a varied array of drilling projects within the foundation drilling industry. He has on the job, technical expertise in dealing with various geologic formations, the problems they pose and the solutions to overcome them. Some of his skills lie in assessment and planning, soils analysis, calculating and designing site specific slurry system programs, estimations, consulting with D.O.T. engineers/inspectors, conducting drilling schools & classroom instruction including ADSC/Union Local 3, on-site slurry preparation/mixing, drilling procedures, trouble shooting, slurry testing procedures, analysis, recycling and disposal, slurry construction/management training. Mike chaired the 2017 Assoc. of Drilled Shaft Contractors ADSC National, Annual Slurry School in St. Petersburg, FL.

Mike has designed calculated slurry programs and worked with most all Category 1-2 as well as 3-4 drilling contractors on many major bridge, structures, & highway construction projects on the West Coast & Western Canada over the years. Mike is currently leading Western States Business Development and is the Lead Slurry Engineering Consultant with PACO Ventures (Pacific American Commercial Company) based out of Seattle, WA. Mike is based out of Ventura, CA.

### **SAMPLE OF PROJECTS - SLURRY PROGRAMS - SALES - CONSULTATION**



Hood Canal Project – Seattle, WA

<http://www.wsdot.wa.gov/projects/sr104hoodcanalbridgeeast/>

Richmond/San Rafael Bridge Project– Bay Area, CA

[www.dot.ca.gov/hq/esc/tollbridge/Rich-SR/Rich-SR.html](http://www.dot.ca.gov/hq/esc/tollbridge/Rich-SR/Rich-SR.html)

Benicia/Martinez Bridge Project – Bay Area, CA

<http://www.dot.ca.gov/dist4/benicia/>

Bay Bridge Project – San Francisco/Oakland CA

<http://www.baybridgeinfo.org/>

Port Mann Bridge Project – Vancouver, BC

<http://www.pmh1project.com/>

Manette Bridge Replacement Project, Bremerton, WA

<http://www.mansonconstruction.com/manette-bridge-replacement/>

Transbay Transit Center Project – San Francisco, CA

<http://transbaycenter.org/>

Schuyler Heim Bridge Replacement Project, Long Beach, CA

<http://www.newgdbbridge.com/>

SR520 Bridge Replacement Project-Seattle, WA

<http://www.wsdot.wa.gov/projects/SR520Bridge/>

San Francisco Central Subway Project, San Francisco, CA

<http://www.hsr.ca.gov/>

California High Speed Rail Project, San Joaquin Valley, CA

<http://www.hsr.ca.gov/>

The Maline Creek Tunnel Storage Facility, St. Louis MO

<http://www.projectclearstl.org/build-system-improvements/maline-creek-storage-facility/>

New Los Angeles Rams Football Stadium, Inglewood, CA

<http://www.cnn.com/2016/01/19/architecture/new-nfl-stadium-los-angeles/>

Metro Purple Line Subway Extension, Beverly Hills, Westwood, Los Angeles, CA

<https://www.metro.net/projects/westside/>



**For consultation or design of a Site-Specific Slurry System Program or training contact**

**Mike Hagy @ (805) 746-6965 [Mike@PacoEquip.com](mailto:Mike@PacoEquip.com)**

# SLURRY BUSTER™ DRY

## SHORE PAC POLYMER SLURRY BREAKER

### DESCRIPTION

SLURRY BUSTER DRY is an industrial grade oxidizing agent used to breakdown SHORE PAC polymer slurry. This white granular solid dissolves completely when applied to SHORE PAC polymer slurry.

The active ingredient is a powerful class III oxidizer that ensures rapid and complete slurry degradation. SLURRY BUSTER DRY is supplied in plastic re-sealable pails. SLURRY BUSTER DRY is a highly effective clean-up solution.

### RECOMMENDED USE

SLURRY BUSTER DRY mixes rapidly into the drilling slurry and breaks the polymer backbone through an oxidation reaction. After treatment with SLURRY BUSTER DRY all that remains is water; ready for convenient disposal. SLURRY BUSTER DRY is designed to be added at the tank or waste pit but never to the excavation.

### CHARACTERISTICS

- No freeze concerns
- Maximum strength at 65% active ingredients
- Easy-to-use re-sealable pails
- Breaks slurry faster for quick, efficient disposal
- Soluble in water
- Will not decompose when stored of properly

### TYPICAL PROPERTIES

Physical State:	Solid Granular
Appearance:	White to off white
Odor:	Chlorine-like
pH:	10.4 - 10.8 (1% solution in neutral, distilled water) (@ 25° C)

### MIXING AND APPLICATION

15 lbs of SLURRY BUSTER DRY per 10,000 gallons SHORE PAC polymer slurry. Circulate entire volume of slurry by pumping to ensure complete oxidation of polymer molecules.

Note: For high viscosity slurry or slurry that has been pre-treated with DE-CHLOR a higher dosage of SLURRY BUSTER DRY may be necessary.

### PACKAGING:

15 lb pail, 36 per pallet. All pallets are plastic-wrapped..

North America: 847.851.1800 | 800.527.9948

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UPDATED: OCTOBER 2013

TDS\_SLURRYBUSTER-DRY\_AM\_EN\_201310\_V1



An **AMCOL** Company

[www.CETCO.com](http://www.CETCO.com)

# USE OF SHORE PAC® POLYMER SLURRY

## IN SLURRY-DISPLACED FOUNDATION CONSTRUCTION



North America: 847.851.1800 | 800.527.9948 | [www.CETCO.com](http://www.CETCO.com)

UPDATED: FEBRUARY 2019

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FORM: CETCO - DRILLING PRODUCTS SHORE PAC DRILLING & MIXING GUIDE



**CETCO®**

## INTRODUCTION

This specification provides direction in the proper use of SHORE PAC® and its additives while improving standardization, quality, and performance in the practice of slurry-displaced deep foundation construction. This document ensures that engineers and engineering geologists can confidently predict the load carrying capacity of the piling being constructed using an approved slurry, and to ensure that an approved slurry is not detrimental to the structural capacity or service life of the piling.

## ADVANTAGES

The advantages of using high performance polymer slurry over mineral slurry yield multiple benefits, which improve construction economics in many ways. SHORE PAC saves time and money while improving construction quality and reducing defects.

- ▶ Controls fluid loss in sands and gravels. Stabilizes excavations
- ▶ Highly concentrated. Very small quantities required
- ▶ Improves productivity of machines and crews
- ▶ Reduces chipping and cleaning of poured concrete
- ▶ Reduces or eliminates disposal costs. Product is environmentally safe
- ▶ Reduces transport costs and storage space requirements
- ▶ Requires less mixing/processing equipment, reducing capital investment, jobsite congestion, and fuel costs

## SCOPE

This specification covers the use of polymer stabilizing support fluids (“slurry”) based on SHORE PAC, an easy mixing, water-soluble, polymer supplied as a free-flowing granular material. SHORE PAC earth-reinforcing fluid is designed for use in the construction of bored piles by the slurry-displacement method.

## SELECTION OF POLYMER SLURRY MATERIALS

The principal polymer is SHORE PAC, manufactured by CETCO. Additives which have been certified by the manufacturer (CETCO) may be used with approval of the engineer and in accordance with the manufacturer’s recommendations. The strict quality control guidelines set forth by the California Department of Transportation (CALTRANS) requirements for approval of SHORE PAC polymer drilling slurry have been applied to ensure the use of proven materials and techniques.

## SHORE PAC POLYMER DOSAGE AND VISCOSITY

SHORE PAC is an easy mixing, water-soluble, polymer supplied as a granular material. SHORE PAC is designed for preparation of viscous earth-reinforcing fluids or slurries for a variety of drilling, trenching, and walling applications in the geo-construction industry.

1. Pre-treat make-up water with SODA ASH 6 lbs per 1,000 gallons make-up water for a pH of 8-10. Pre-treat make-up water with DE-CHLOR 0.5 lb per 1,000 gallons mix water.
2. Add SHORE PAC through a Venturi type mixer at 3.4-10.0 lbs per 1,000 gallons depending on desired viscosity if mixing in surface tank, if mixing directly within excavation sprinkle into stream of water slowly.
3. Take a Marsh Funnel Viscosity reading. Viscosity should be 35-125 sec/qt.

SHORE PAC dosage and the viscosity of the slurry shall be selected and controlled within ranges which suit the soil and mix water conditions of the work and according to table 3.1.

Table 3.1

FORMATION TYPE	SHORE PAC DOSAGE OR CONCENTRATION			MARSH FUNNEL VISCOSITY
	Lbs/yd <sup>3</sup>	Lbs/1,000 gals	Kg/m <sup>3</sup>	Sec/qt
Clay & Shale	0.7 - 0.8	3.5 - 5.0	0.5 - 0.6	35 - 50
Silt & Fine to Med. Sand	0.8 - 1.0	5.0 - 7.0	0.6 - 0.8	50 - 70
Coarse Sand to Pea Gravel	1.2 - 1.5	7.0 - 9.0	0.8 - 1.0	70 - 90
Gravel to Cobble	1.7 - 2.4	9.0 - 12.5	1.0 - 1.5	90 - 125



## MAKE-UP WATER AND EFFICIENT SLURRY PRODUCTION

Sufficient water supply of proper quality for slurry make-up water shall always be available to support planned operations and unknown contingencies. Slurry mixing capability shall be immediately and continuously available to support planned operations and unexpected events. If the water supply is from a low-rate or irregular source such as a small well, a small diameter supply line, or tanker truck, a tank for storage of water shall be used to guarantee adequate and uninterrupted slurry making capacity.

SODA ASH should be used to adjust the pH and treat out calcium (Ca) and magnesium (Mg) contaminants that are detrimental to polymers. SODA ASH will adjust the pH of the mix water to between 8 and 10, which is optimum for SHORE PAC performance. The ratio of SODA ASH to water is 6 lbs per 1,000 gallons of water.

The additive DE-CHLOR is used to treat out chlorine (Cl) if municipal water is used for make-up water. Chlorine, present in municipal water, destroys all polymer molecules and decreases its viscosity if chlorine registers greater than 3 ppm. DE-CHLOR is a cost effective white granular crystal that neutralizes chlorine in municipal water and is environmentally safe. The ratio of DE-CHLOR to water is 0.5 lb per 1,000 gallons of mix water.

## CONTAMINATES

Polymer slurries are sensitive to various contaminants, which occur in groundwater, soil, cement, and make-up water. Petroleum hydrocarbons, calcium, acidity, alkalinity, chlorine, and sodium chloride are some contaminants that will affect the polymer slurry. These contaminants are often introduced into the slurry from the soil, groundwater, and/or industrial wastes at the construction site. There is a need to identify and correct these problems for a smooth operation to take place. This begins with geotechnical engineers in the site investigation process. Identification and documentation should be present with soil logs and passed onto the general contractor and subcontractors. The procurement of samples of groundwater and the analysis of such samples for pH and contaminants should become a standard part of subsoil investigations conducted by geotechnical drilling service firms or by your own investigation. When contamination is present or buffering is required, additives shall be used in accordance with manufacturer's recommendations.

## MIXING SHORE PAC

SHORE PAC polymer may be mixed pre-mixed in surface vessels or mixed directly within the excavation. The mix water or the prepared fluid shall be treated with appropriate additives as specified by the manufacturer.

## MIXING DIRECTLY IN EXCAVATION

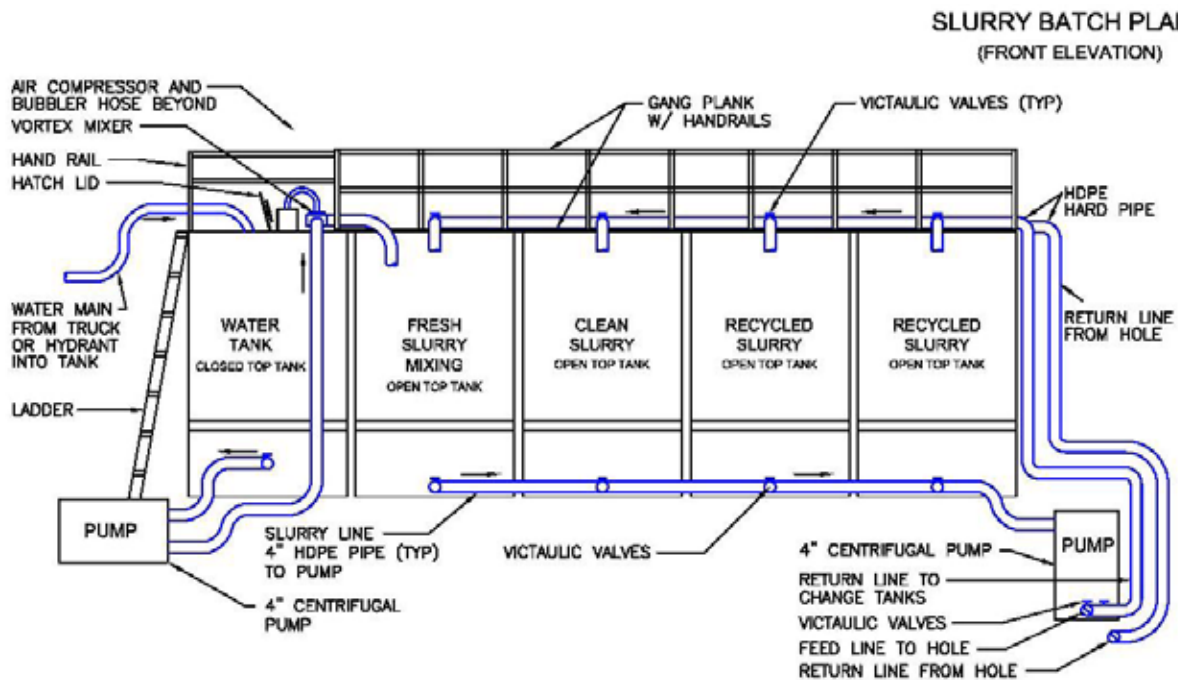
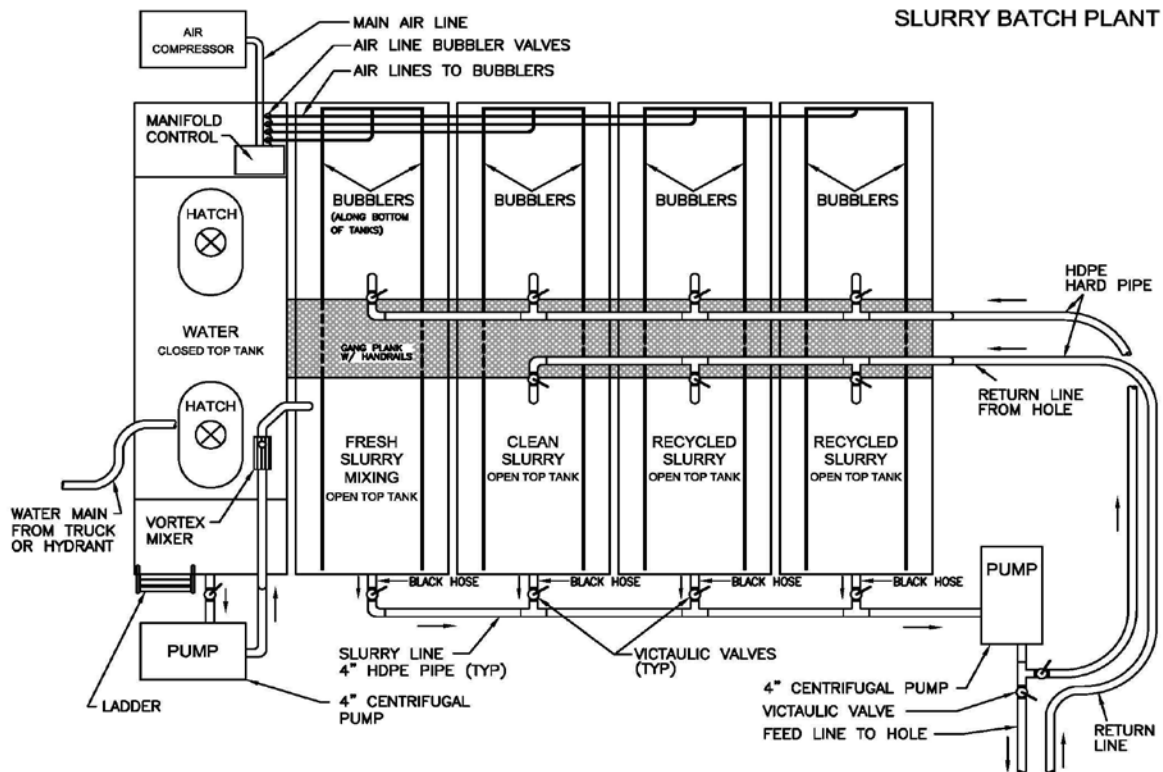
When mixing directly in the excavation it is important to have a steady stream of water that is positioned to provide a point of rapid and wide water flow for introduction of the polymer by sprinkling or sifting. Mixing of fresh polymer shall be completed by sprinkling or sifting the polymer carefully onto a flowing stream of water or fluid from a pressurized source directed into the excavation, such that the flowing fluid catches, wets, and separates the polymer grains so that they disperse and hydrate as individual particles, avoiding the forming of lumps or balls of un-mixed polymer. Dry polymer shall not be added directly onto the fluid in the excavation (as opposed to being added on a flowing stream) because this normally produces lumps or "fisheyes." The additive ACCU-VIS will create instant viscosity with out having to shear.

When a new polymer mix is being prepared in a hole that has been dug or drilled to significant depth before adding slurry, the excavation shall be filled with water to a water column height (measured from bottom of excavation) of no less than two meters or 15% of excavation depth, whichever is the greater, before beginning to add the polymer. SHORE PAC dry granular polymer shall be added at a controlled rate on the stream of water that is filling the hole in order to avoid lumps and fisheyes. The excavating tool (auger, bucket, clamshell) shall be reciprocated gently the full length of the slurry column while the polymer is being added, to distribute and even out the fresh polymer, and to ensure that none of the polymer settles to the bottom of the excavation during the mixing and thickening process.

When adding fresh dry polymer to recycled fluid directly in the excavation, special care must be taken to ensure good dispersion of the polymer grains to avoid forming lumps. This is because the polymer wets-out and disperses more slowly in thickened fluid than in plain water. Fanning the recycled fluid across an auger or other object to provide a point of wide and rapid flow facilitates the adding of fresh dry polymer.

## MIXING IN VESSELS OR TANKS

When SHORE PAC polymer is pre-mixed in vessels it shall be added to water that is being passed through a hose, tube or hopper, across a stationary panel or surface, or stirred or otherwise agitated, in a manner which avoids the formation of lumps and results in a uniform mixture of polymer in the water. The polymer slurry shall be agitated until it develops viscosity adequate to be self-suspending (i.e., particles of partially-dissolved polymer do not settle in the fluid). This normally occurs within 15 to 30 minutes. Polymer shall not be mixed in a vessel without adequate agitation. Agitation may be accomplished by use of motorized stirrers, air injection, (as with blowpipes or fixed perforated piping), or other suitable and effective means. Recirculation by a single pump (without other means of agitation) is usually inadequate and shall not be permitted unless the mix tank is small enough that the pump provides adequate agitation of the entire tank.





## ADDITIVES

CETCO has developed a complete line of additives as companion products for SHORE PAC when problem conditions arise. Additives shall be used in accordance with recommendations listed in the table to the right. Control guidelines for use of these additives shall be pH, chlorine levels, contaminant levels, fluid behavior, and other parameters as specified by manufacturer.

This system based on the SHORE PAC polymer and specialized additives, has a track record of delivering the highest levels of performance and project economy of any slurry technology on the market including bentonite.

With this system you can stabilize the most challenging of formation conditions, cohesion-less sands, open corals, cobbles, etc., thereby eliminating collapses and controlling fluid loss. This results in reducing concrete over-breaks, saving on the quantity of concrete consumed, polymer consumed, and the time required for drilling while providing the highest levels of skin friction and rebar bonding available with a slurry system.

## MAINTENANCE

The slurry level shall be maintained at least 1.8 meters (six feet) above the water table, or as such higher level that is required to overbalance hydrostatic soil pore pressure and maintain soil stability. If the slurry drops below the specified level, the operation shall be paused and the proper slurry level re-established before proceeding. In some situations the manufacturer may recommend that the slurry be maintained at less than 1.8 meters (six feet) above the water table, to reduce rates of fluid loss if soil stability is being maintained.

The point of reference for selection and maintenance of slurry level shall always be the water table (piezometric level). This applies even in situations where casing or other protective sleeve has been placed to a depth at or below the water table. The presence of casing does not remove the requirement to keep the slurry level above the water table. Attempts to excavate or hold open an excavation in saturated or unstable soils with inadequate slurry head pressure; even with casing extended into the water table, can be expected to result in soil collapse below the casing.

## SAMPLING AND TESTING

Samples of the slurry shall be taken from near-bottom of the excavation, from the upper portion of the excavation, and from the slurry supply tanks (if applicable) at regular intervals during the excavating process in order to facilitate control of slurry properties.

PRODUCT	RECOMMENDED DOSAGE RATE	DESCRIPTION	FUNCTION
ACCU-VIS	Add 2-3 gals in weighted sealed plastic bag to desired area. Break open with auger and mix with drill tool	Liquid anionic polymer	Stabilizes loose granular soil, instant viscosity, no need to shear with fluid
DE-CHLOR	0.5-1.0 lbs/1,000 gals mix water	Dry chlorine neutralizer	Treats chlorine in municipal water, increases yield and performance of slurry
INSTA-CLEAR DRY	40 lbs/3,000 gals mix water	Reactive separating agent	When added into slurry acts instantly to settle suspended fines
MACRO-FILL	Add 15 lbs 1 pail directly into excavation around the circumference	Dry super-absorbent material	Controls slurry loss in extreme conditions
SAND SEALANT/ MULTI-SEAL	30 gals water or slurry, ½ bag of SAND SEALANT, and a ½ bag of MULTI-SEAL	Natural mineral solid combined with a select blend of four types of materials	Treats advanced fluid loss situations
SHORE PAC X	1-5 lbs SHORE PAC X per 1,000 gallons SHORE PAC slurry	Specially synthesized polymer nano composite	Fluid Loss Additive
SLURRY BUSTER DRY	15 lbs of SLURRY BUSTER DRY per 10,000 gallons SHORE PAC polymer slurry	Industrial grade oxidizing agent	Breaks slurry to water
SODA ASH	6 lbs/1,000 gals mix water	Dry pH adjuster	Optimizes polymer performance and yield
SODIUM BICARBONATE	5 lbs/1,000 gals mix water	A buffer used to lower pH	Treats slurry impacted by concrete
CETCO CRUMBLES/ STONE STOP	Add into hole to stop slurry loss	8-20 mesh granular sealant	Controls slurry loss in extreme conditions

## SAMPLING AND TESTING (CONT'D)

During the excavation of the borehole, slurry samples shall be taken from near-bottom and upper portion at least once during the excavation, and not less than once every four hours, except for overnight shutdowns. When operating conditions make it prudent to sample and test more frequently, sampling and testing shall be done in accordance with a schedule recommended by the manufacturer or the contractor and approved by the Engineer.

Samples shall be collected with a suitable device (double ball bailer) that captures representative samples of sufficient volume ( $\geq 1.8$  liters or 2 quarts) to perform required testing of the slurry. Samples collected as described above shall be tested for Marsh Funnel Viscosity, pH, and specific weight. A written record shall be maintained, showing viscosities, pH values, specific weights, dates, times, excavation identifiers, depths, and locations from which samples were taken (excavation, supply tank, mix tank) and other pertinent information as specified by the Engineer. Testing of specific weight and sand content may be required by the Engineer before placement of reinforcing steel and concrete, if specifications for these parameters are in force for the project.

## FLUID LOSS

If high rates of fluid loss (seepage of slurry into the soil) are encountered, the polymer dosage and viscosity of the slurry shall be increased as required to provide adequate control of fluid loss consistent with allowed ranges of slurry viscosity. Alternatively or additionally, fluid loss control agents or other treatments recommended by the manufacturer may be used. Use only additives that are certified by the manufacturer to be compatible with the slurry in use.

STONE STOP is a specially blended mineral used for fluid loss control especially in sandy soils. STONE STOP added to SHORE PAC reduces slurry seepage into saturated open sands and gravels. A granular solid, STONE STOP, is highly recommended as an additive to SHORE PAC when drilling in loose saturated sands. When cobble or gravel is encountered, the viscosity may need to be increased to help prevent loss of fluid to these possible theft zones.

If losses are severe, it may be necessary to add ACCU-VIS to the slurry to either rapidly gain viscosity or use it as a "Bomb" to cut losses. ACCU-VIS can boost cohesion of sand, gravel, and cobble to stabilize and control slurry loss to a degree. ACCU-VIS sharply reduces slurry loss rates in very coarse soils and reduces bottom hole cleaning time. ACCU-VIS's thick gelatinous texture combines with fines to assist in plugging up the theft zones and helps to hold back heaving sand. The application for ACCU-VIS is 1 gallon per 1,000 gallons of fluid. It can be dropped down in weighted, thin, plastic bags, which can be torn up and mixed by the drilling tool.

ACCU-VIS may also be poured into the top of the hole, as it will mix and become viscous without having to shear by force of fluid. ACCU-VIS can be mixed and distributed through the shaft with the drilling tool without forming fisheyes.

## SPECIFIC WEIGHT OF THE SLURRY

Because the primary polymers of the standard SHORE PAC system add no significant weight to slurry, measurement of slurry specific weight is a direct indicator of the soil solids content (sand, silt, clay) of the slurry. Sand content is dealt with by a sand specification. Sand tends to settle to the bottom of the excavation because the SHORE PAC polymer slurry has no tendency to gel, so temporary or transient elevated sand content is not a problem during the excavation process. Aside from sand present in the slurry, the remainder of the slurry's specific weight above the specific weight of water (1.00 kilogram per liter, 62.4 lbs/ft<sup>3</sup>, or 8.35 lbs/gal) comes from soil fines dispersed in the slurry. Consequently, the slurry specific weight specification is in effect a limiting factor on the amount of fines that are acceptable in the slurry. High fines content can cause problems if the fines are not held in stable suspension. The slowly-settling fines can create a bed of sediment on the bottom of the excavation after a period of time. The maximum allowable final specific weight for synthetic polymer slurries, according to the present specification, is listed in the specification table.

## PREPARATION FOR CONCRETE PLACEMENT

Upon reaching final depth, an initial cleaning of the bottom of the excavation shall be effected with an appropriate tool. If indicated, the slurry column shall be allowed to stand static and undisturbed for a period of time to allow sand to settle toward the bottom of the hole. Slurry samples shall be taken intermittently during this static period from the midpoint of the excavation and from within 60 centimeters of bottom to determine sand content, viscosity, pH, and specific weight. When sand content and specific weight of near-bottom and midpoint samples are within specified maximums (see slurry quality specification tables) or when they stabilize and show no further change over a 30-minute interval during which the excavation is completely static and if tools have not been inserted (indicating sand held in stable suspension), the bottom of the excavation shall be cleaned and placement of rebar and concrete may proceed.

If the sand-size particles in the fluid are not in stable suspension but are settling very slowly, other measures may be required. For example, adjusting the fluid properties to stabilize the suspension and keep the sand from settling; agglomerating soil particles into masses (which can be extracted by the excavating tools), exchanging the fluid in the excavation with clean fluid, treating the slurry with additives to accelerate settling, or otherwise enhance removal of suspended soil.

## ELAPSED TIME BETWEEN BOTTOM-CLEANING AND PLACEMENT OF CONCRETE

Not more than 120 minutes shall elapse between the final cleaning of the bottom of the excavation and the initiation of concrete placement, unless an exception is approved by the Engineer.

## TESTING OF SHORE PAC POLYMER SLURRY

### MARSH FUNNEL VISCOSITY (MFV)

#### EQUIPMENT

1. Marsh Funnel
2. Graduated one quart viscosity cup
3. Stopwatch

#### PROCEDURE

1. Use a double ball bailer to retrieve approximately 2 quarts of slurry.
2. Check the Marsh Funnel to verify that there is no obstruction in the outlet at the bottom of the funnel and the slurry will have an unobstructed flow. Hold funnel upright with a finger over the outlet. Pour the test sample through the screen in the top of the funnel until the mud level just reaches the under side of the screen.
3. Hold the funnel over the viscosity cup and release finger from the outlet and start timing. Record the amount of time in seconds it takes to fill up one quart.
4. Record time in sec/quart on slurry test report.

This test requires both a Marsh Funnel and a Viscosity Cup. MFV is reported in seconds per quart. The time in seconds for a quart of slurry to pass through the funnel tip is reported as viscosity in seconds per quart. MFV is very useful in determining the concentration of polymer molecules, and also its ability to stabilize surrounding soils.

### pH (POTENTIAL HYDROGEN- ION)

#### EQUIPMENT

1. pH Indicator Paper

#### PROCEDURE

1. Dip a piece of pH indicator paper into the slurry and compare the color change to a standard chart. The result of this test is reported in a number from 1 to 14.
2. Record pH on slurry test report.

In this test, the range for maximum SHORE PAC performance is 8-10. This is the level at which polymer molecules can fully hydrate and extend, creating more viscosity. Levels of pH below 6 (acidic) can affect the performance of the SHORE PAC slurry and should be adjusted by adding SODA ASH, 6 lbs per 1,000 gallons mix water. In addition, the sodium carbonate ion present in 8-10 pH solutions is useful in buffering the slurry against calcium and magnesium contamination.

## TESTING OF SHORE PAC POLYMER SLURRY (CONT'D)

### SAND CONTENT DETERMINATION

#### EQUIPMENT

1. 200-mesh sieve
2. Funnel to fit into sieve
3. Glass sand content tube
4. Wash bottle

#### PROCEDURE

1. Fill the sand content tube with slurry to the first line marked "mud to here" then fill the remaining space in the tube to the next line marked "water to here". Place your thumb over opening and shake vigorously, inverting several times.
2. Pour the mixture on to the clean, wet screen. Discard the liquid passing through the screen. Add more water to the tube, shake, and pour onto the screen again. Repeat this until tube rinses clean. Wash the sand on the screen until discard water is clear, this removes any remaining silt and clay.
3. Fit the funnel upside down over the top of the screen. Slowly invert the assembly and insert the tip of the funnel into the glass sand content tube. Wash the sand into the tube by spraying a fine stream with the wash bottle making sure not overflow the tube (tapping the sides of the screen may facilitate this process).
4. Allow the sand to settle, from the gradations on the tube, read the volume percent of the sand and record it on the slurry test report.

This test is performed with a standard sand content kit, and the results are reported as percent sand. This test is normally performed at the completion of an excavation and just prior to placing concrete. The sample to be tested should be taken near the bottom of the excavation. When using SHORE PAC slurries the sand content will rarely test over 1.0% sand. Due to its flocculating ability, it drops the sand very quickly and the slurry remains nearly sand free. When performing the sand content test in the field the addition of SLURRY BUSTER solution in place of water to dilute the slurry sample can prevent the accumulation of silt, which creates false sand reading in the test.

### SPECIFIC WEIGHT (DENSITY)

#### EQUIPMENT

1. Mud balance with base and cap per API spec 13B-1, Sec 1

#### PROCEDURE

1. Place mud balance on a flat level surface and make sure it is clean of any caked on debris.
2. Fill the cup with the slurry to be tested and place the lid on the cup, seat it firmly but slowly with a twisting motion. Be sure some mud runs out of the hole in the cap to free any trapped air.
3. With the hole in the cap covered with one finger, wash and wipe all of the slurry from the outside of the cup and arm of the balance.
4. Set the arm on the fulcrum base and move the sliding weight along the graduated arm until the cup and arm are balanced.
5. Read the density of the mud at the left edge of the sliding weight.
6. Report the results on the slurry test report to the nearest scale division in lb/gal, lb/ft<sup>3</sup>, S.G., or psi/1,000 ft of depth.
7. Wash the mud from the cup immediately after each use. It is absolutely essential that all parts of the mud balance be kept clean for accurate results to be obtained.

This test is performed with a standard mud balance and is reported as specific gravity, pounds per cubic foot or pounds per gallon. The lbs density of SHORE PAC slurry should be approximately 64.0 lbs/ft<sup>3</sup>. The density may be slightly higher depending on the amount of fine soil particles mixed in the slurry. SHORE PAC slurries have the same density as water, specific gravity 1.0 (± 0.05).

**DRILLING CONTRACTOR:** \_\_\_\_\_

**SLURRY ENGINEER:** \_\_\_\_\_

**CONTRACT #:** \_\_\_\_\_

**DATE:** \_\_\_\_\_

**PROJECT INSPECTOR:** \_\_\_\_\_

**SHAFT #:** \_\_\_\_\_

**DIAMETER:** \_\_\_\_\_

**T.D. DEPTH:** \_\_\_\_\_

**HOLE VOLUME:** \_\_\_\_\_

**PRODUCTS ADDED:** \_\_\_\_\_

TESTS PERFORMED	SAMPLE #1	SAMPLE #2	SAMPLE #3	SAMPLE #4
Time				
Depth (Feet)				
pH (1-14)				
Marsh Funnel Viscosity (Sec/qt)				
Density (lb/gal)				
Sand Content (%)				
Soil Conditions				

**COMMENTS:** \_\_\_\_\_

**CETCO REPRESENTATIVE/SLURRY ENGINEER:** \_\_\_\_\_

## QUALITY SPECIFICATIONS FOR SLURRIES BASED ON SHORE PAC

SHORE PAC POLYMER SLURRY		
Property	Requirement	Test
Density (lb/ft <sup>3</sup> ) - just prior to placing concrete	less than or equal to 64*	Mud Weight (Density) API 13 B-1 Section 1
Viscosity (seconds/quart)	35 to 135	Marsh Funnel and Cup API 13 B-1 Section 2.2
pH	8.0 to 10.0	Glass Electrode pH Meter or pH Paper
Sand Content (%) - just prior to placing concrete	less than or equal to 1.0%	Sand API 13 B-1 Section 5
*When approved by the engineer, slurry may be used in saltwater, and the allowable densities may be increased up to 2 pcf. Slurry temperature shall be at least 4 °C (40 °F) when tested.		

SHORE PAC is not a hazardous waste, nor does it pose any threat to waters when disposed of according to manufacturer's guidelines.

SHORE PAC is approved for use by The Federal Highway Administration, (FHWA) and is used in State Departments of Transportation throughout the nation. The method for disposing the drilling slurry SHORE PAC on Drilled Shaft Projects has been listed within this correspondence.

## DEFINITION AND INGREDIENTS OF SHORE PAC

SHORE PAC is a dry granular synthetic anionic polyacrylamide. SHORE PAC is manufactured from co-polymerization of acrylimide and acrylic acid or its inorganic salts. The molecular weight (in the region of several million Daltons) and negative charge density varies (by variation of the ratio of acrylimide and acrylic acid monomer units).

The polymer used in the product SHORE PAC is designated as non hazardous and is water soluble or water dispersible. The term polymer simply means – many parts, or is an organic chemical having a molecular weight above 200, with greater than eight repeating units. Polymers vary greatly in function and basic properties, such as stability, charge, and molecular weight. In general, polymers can be classified as natural, modified-natural, or synthetic. The term “monomer” simply means – a large molecule made up of simple repeating units.

A polymer is a compound that consists of a chain of repeating base units, called monomers. SHORE PAC is a synthetic polymer.

## DEFINITION AND INGREDIENTS OF SHORE PAC

SHORE PAC is a very high molecular weight synthetic polymer with negative charges on the backbone. Its high molecular weight gives viscosity to water at low concentrations.

When SHORE PAC is dissolved in aqueous solution, the very long polymer chains dissolve and orient randomly in the fluid in coils. In freshwater, the repulsion of the negative charges on the backbone of the polymer chains causes the coils to expand and to occupy a large volume in the fluid. When the fluid is sheared, the expanded polymer chains are located in different fluid layers in the shear field. The uncoiling of these expanded polymer chains dissipates mechanical energy and results in viscosity.

The high molecular weight polymer chains are so long that different parts of individual polymer chains bridge different solid particles. It is this adsorption on surfaces and bridging of solid surfaces that makes this polymer effective in keeping solids consolidated while drilling a foundation. In addition, the adsorbed layer of hydrophilic polymer on rock surfaces slows down the diffusion of water into the rock.

## CONTROL PRESSURE AND STABILIZE THE BOREHOLE

Two types of pressure are exerted on the borehole during drilling, formation pressure and hydrostatic pressure. Formation pressure can collapse the borehole if it is not overcome by hydrostatic pressure pushing back against the formation. Hydrostatic pressure is the weight or density of the volume of drilling slurry pushing against the formation. In order to have hydrostatic pressure, the drilling slurry must push back against the formation with minimal penetration into the formation. In unconsolidated permeable formations, the hydrostatic pressure occurs when the weight of the fluid is in contact with the impermeable deposits (filter cake) placed on the sides of the borehole by the drilling slurry. The filter cake and the hydrostatic pressure thereby control the formation pressure, reduce slurry loss and prevent caving, resulting in hole stabilization.



## QUALITY SPECIFICATIONS FOR SLURRIES BASED ON SHORE PAC

Normal water weighs 8.34 lb/gal, with the SHORE PAC polymer fluid at 8.40 lb/gal it is necessary to maintain the slurry level 2 to 3 meters (7 to 10 feet) above the surrounding groundwater level. Under normal conditions this 2 to 3 meters of hydrostatic pressure, or head, exerts the pressure necessary (approx. 450 to 640 lb/ft<sup>2</sup>, or 2,000 to 3,000 kg/m<sup>2</sup>), to support the walls of the excavation and is required to ensure hole stability. Without this positive pressure exerted by the slurry column against the sidewall, soil overburden pressures will cause the excavation to collapse. The natural soil overburden pressures forced against the positive pressure exerted by the slurry column result in little or no leach ability to the surrounding formation.

## RECYCLING OF THE SHORE PAC SLURRY

After the slurry testing has been completed and the rebar has been placed, a suction line should be dropped just inside the excavation for recycling of the slurry. While the concrete is being tremied it will displace the slurry forcing it upward. A holding tank large enough to hold the volume of slurry contained within the excavation is required to recycle the SHORE PAC slurry. When concrete is tremie pumped into the bottom of the hole, the displaced SHORE PAC slurry is pumped from the top of the excavation into the holding tank using a centrifugal pump. Disregard concerns about shearing the polymer and destroying it, this is the only pump that will pump a large enough volume to keep-up with the concreted pump truck.

Avoid pumping the last three feet of slurry above the concrete interface, as this slurry will be contaminated from contact with the concrete. The impacted slurry looks like oatmeal and only occurs at the contact with the concrete. The last three feet of impacted slurry should be pumped off to a waste tank, or if allowed the cement contaminated slurry can be released over the top can onto the ground to be mixed into the spoil pile by the loader.

The recycled SHORE PAC slurry is tested for viscosity and pH. While adding water to restore the original volume additional SODA ASH is added to adjust the pH. Next the SHORE PAC is added to restore the slurry to full strength. Usually it requires about ¼ of the amount of SHORE PAC added to the water filling up the holding tank to restore the slurry to its original strength for reuse on the next hole.

## BREAKDOWN OF SLURRY

SHORE PAC slurry fluids are non-toxic and are readily degradable upon completion of a project to facilitate disposal. Upon completion of the project, any remaining SHORE PAC is broken down with the chemical oxidizers. SLURRY BUSTER DRY is the most common oxidizer for this purpose. SLURRY BUSTER DRY is calcium hypochlorite.

SLURRY BUSTER DRY is added to the SHORE PAC slurry at a rate of 15 lbs per 10,000 gallons of SHORE PAC slurry. This is accomplished by pumping it back into a holding tank or holding pond and circulating it using the pumps on-site to ensure complete oxidation of the polymer molecules.

SLURRY BUSTER DRY concentrations of 15 lbs per 10,000 gallons of SHORE PAC destroys the active ingredients within the sodium hypochlorite (bleach) and at the same time breaks the polymer, reverting it back to basic water. The end result of SHORE PAC decomposing after its encounter with SLURRY BUSTER DRY is the acrylic acid backbone which is an inert nontoxic substance.

## DISPOSAL OF DRILLING SLURRY

Treated slurry fluids are environmentally safe when handled as directed. When breakdown is complete, all that remains is trace acrylate molecules, water and perhaps some small amount of excess chlorine. The anionic SHORE PAC is reduced to water after the hypochlorite is used to treat the SHORE PAC. This is often safely discharged, or spread on the ground to evaporate, or used in dust control.

Additionally, polymers with the same chemical base as found in SHORE PAC are used in potable water treatment as flocculants, with federal government clearance. They are widely used throughout the world as coagulants and flocculants used for environmental and process improvement, acting through solid/liquid separation. They are used in paper manufacturing, wastewater treatment, mineral and oil extraction, soil conditioning, and as thickeners in cosmetics. As such, they have many regulatory approvals around the world, such as for drinking water treatment, indirect additives for food-contact paper, and for other specific uses. Municipal sewage sludge, which has been polymer-treated for dewatering, is widely applied to agricultural land.

**MICHEL'S®**

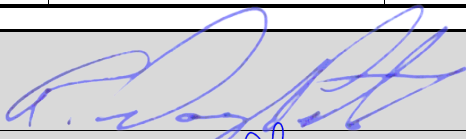

**FOUNDATIONS**



**TAB 5**

Contract:  9242	Subcontractor:	For (Location) Project Wide Use	RAM NUMBER:
	Date:	Transmittal Package No. FLJV-WTRN-9242-00441	

ROM #	Material or Manufacturer's Product/Type	Name and Location of Fabricator, Manufacturer or Pit Number	Unit Of Measure	WSDOT Specs Reference	RAM Approval Action Code	QPL	Requirements
						Listed on QPL Yes No  QPL Code:	MCC Mill Cert Test Rpt. Cat. Cuts Shop Drw. Stamp/Tag
						Listed on QPL Yes No  QPL Code:	MCC Mill Cert Test Rpt. Cat. Cuts Shop Drw. Stamp/Tag
						Listed on QPL Yes No  QPL Code:	MCC Mill Cert Test Rpt. Cat. Cuts Shop Drw. Stamp/Tag
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						Listed on QPL Yes No  QPL Code:	MCC Mill Cert Test Rpt. Cat. Cuts Shop Drw. Stamp/Tag

Material Approval Engineer		Date
Construction Quality Assurance Manager		Date

### Approval Action Codes for use by QA/QC & State Materials Laboratory

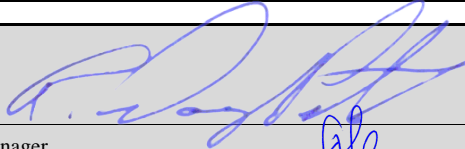

- Acceptance Criteria: Acceptance based upon 'Satisfactory' Test Report for samples of materials to be incorporated into project.
- Acceptance Criteria: Mfg. Cert. of Compliance for 'Acceptance' prior to use of material.
- Acceptance Criteria: Catalog Cuts for 'Acceptance' prior to use of material.
- Acceptance Criteria: Submit Shop Drawings for 'Approval' prior to fabrication of material.
- Acceptance Criteria: Only 'Approved for Shipment', 'WSDOT Inspected' or 'Fabrication Approved Decal' material shall be used.
- Acceptance Criteria: Submit Certificate of Materials Origin.
- Acceptance Criteria: Request Transmitted to State Materials Laboratory for Approval Action.
- Source Approved: Visually Verify Material is As Approved.
- Approval Withheld: Submit samples for preliminary evaluation.
- Approval Withheld:
- Miscellaneous Acceptance Criteria:

### Remarks:

\*See attached Stoneway letter dated February 11, 2021 regarding Mill Cert designation for Ashgrove Cement.

Contract:  9242	Subcontractor:	For (Location) Project Wide Use	RAM NUMBER:
	Date:	Transmittal Package No. FLJV-WTRN-9242-00441	

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Material Approval Engineer		Date
Construction Quality Assurance Manager		Date

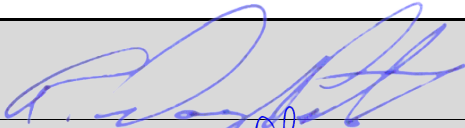

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**Remarks:**

Contract:  9242	Subcontractor:	For (Location) Project Wide Use	RAM NUMBER:
	Date:	Transmittal Package No. FLJV-WTRN-9242-00441	

ROM #	Material or Manufacturer's Product/Type	Name and Location of Fabricator, Manufacturer or Pit Number	Unit Of Measure	WSDOT Specs Reference	RAM Approval Action Code	QPL	Requirements
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Material Approval Engineer		Date
Construction Quality Assurance Manager		Date

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- Approval Withheld: Submit samples for preliminary evaluation.
- Approval Withheld:
- Miscellaneous Acceptance Criteria:

**Remarks:**



# Concrete Mix Design

Contractor Project Wide All Contractors		Submitted By Adam Gaunt - Stoneway Concrete		Date 01/18/2021	
Concrete Supplier Stoneway Concrete			Plant Location East Marginal Way, Seattle		
Contract Number 9242		Contract Name I405 Renton To Bellevue			

This mix is to be used in the following Bid Item No(s): \_\_\_\_\_

Concrete Class: Other - Define in Remarks

Remarks

Class 5000P

Recycled water to be used at 50% unless specified at time of order, extra charges may apply

Mix Design No. CL4KP

Plant No. 11

Cementitious Materials	Source	Plant	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Ashgrove	Seattle, WA	ASTM C 595 Type IL (X) _____	3.1	600
Fly Ash <sup>a</sup>			<input type="checkbox"/> F <input type="checkbox"/> C Alkali % _____		
GGBFS (Slag) <sup>a</sup>	Lafarge NA	Seattle, WA	<input checked="" type="checkbox"/> 100 <input type="checkbox"/> 120	2.87	181

Concrete Admixtures	Manufacturer	Product	Est. Range (oz/cy)
Air Entrainment			
Water-Reducing Type A	GCP Applied Technologies	Zyla 630	1-50
Water-Reducing and Retarding Type D	GCP Applied Technologies	Recover	1-50

Water (Maximum) 312 lbs/cy

Is any of the water Recycled or Reclaimed? ☒ Yes<sup>d</sup> ☐ No

Water Cementitious Ratio (Maximum) 0.40

Mix Design Density (pcf) 147.8

## Design Performance (Attach Test Data)

Average 28-day compressive strength (psi) 8020

Average 14-day flexural strength (psi) (Concrete Pavement Only)

Concrete Chloride Ion Content (% by mass of cement) .0094

☐ Water Soluble ☒ Acid Soluble

## Agency Use Only (Check appropriate Box)

☒ This Mix Design MEETS CONTRACT SPECIFICATIONS and may be used on the bid items noted above

☐ This Mix Design DOES NOT MEET CONTRACT SPECIFICATIONS and is being returned for corrections

Reviewed By: \_\_\_\_\_

2/17/2021

PE Signature

Date

Mix Design No. CL4KPPlant No. 11Aggregate Gradation ☒ AASHTO ☐ CombinedNominal Maximum Size (In) 3/8

Aggregates	1	2	3	4	5	Total
WSDOT Source No. <sup>b</sup>	B335	B335				
Source Expiration Date <sup>b</sup>	03/09/25	03/09/25				
ASR Expansion (%) <sup>b</sup> <input type="checkbox"/> 14 Day <input checked="" type="checkbox"/> 1 Year	.03	.03				
Is ASR Mitigation Required?	NO	NO				
Stock Pile Grading <sup>c</sup>	#8	Class 1				
Percent of Total Aggregate	55	45				100
Specific Gravity (SSD)	2.69	2.66				
Lbs/cy (ssd)	1611	1320				2931
<b>Include Percent Passing for each aggregate component. Include Total only for Combined Gradations.</b>	<b>Percent Passing</b>					<b>Total</b>
2 inch	100.00	100.00				100.00
1-1/2 inch	100.00	100.00				100.00
1 inch	100.00	100.00				100.00
3/4 inch	100.00	100.00				100.00
1/2 inch	100.00	100.00				100.00
3/8 inch	92.00	100.00				95.60
No. 4	25.00	100.00				58.78
No. 8	2.00	85.00				39.38
No. 16	1.00	63.00				28.92
No. 30	0.00	38.00				17.11
No. 50	0.00	15.00				6.76
No. 100	0.00	5.00				2.25
No. 200	0.00	2.00				0.90

Fineness Modulus: (Required for Class 2 Sand)

Proposed ASR Mitigation Method:

**Notes:**

- a Fly ash or GGBFS is required for Class 4000P mix.
- b Enter data from WSDOT ASA Database. ASR Mitigation is required for sources with 14-day expansions greater than 0.20%. No mitigation is required if the 1-year expansion is less than 0.04%. Proposed mitigation methods for 14-day expansions greater than 0.45% require ASTM C 1567 tests proving that the method is effective. See WSDOT Standard Specification 9-03.1.
- c Stockpile gradation: AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation stockpile sizes. See WSDOT Standard Specification 9-03.1.
- d Attach test results indicating conformance to Standard Specification 9-25.1.



Date: 1/18/2021



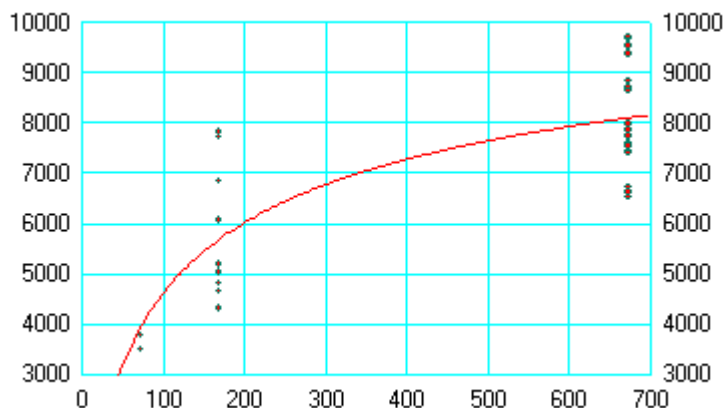
**Stoneway Concrete**  
Where Quality Counts

9216 8th AVENUE S  
SEATTLE, WA 98108  
OFFICE:(425)226-1000  
FAX:(425)228-4924

**Mix Name: CL4KP**

Units : US

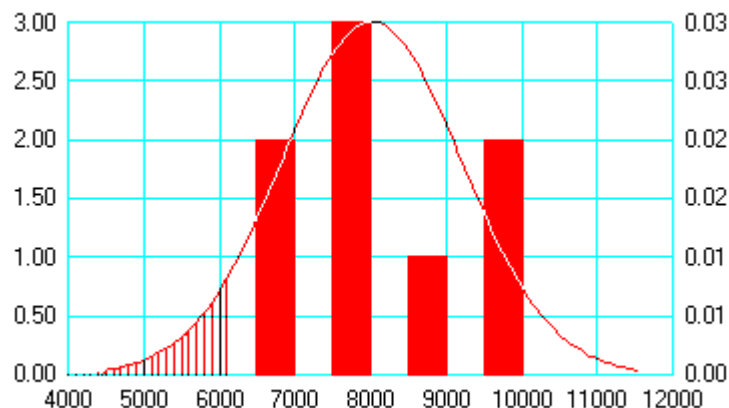
PSI Strength and Strength Fit vs Maturity



Maturity Hours

PSI # of Occ.

Histogram for 28 Day Strength



PSI

95% of tests lie above cross-hatched area

STRENGTH SUMMARY, Compression  
Strengths

Either 4" x 8" Or 6" x 12"

No. Of Tests	Avg Slump	Avg Air	Avg 3 Day	Avg 7 Day	Avg 28 Day	Avg 56 Day	Avg Acc Age	Accept Age
8	8.00	1.30	3650	5540	8020		8020	28

Std ACI318  
Dev Req'd  
-----  
6200

DETAILED STRENGTH, Compression

Either 4" x 8" Or 6" x 12"

Mix Number	Test Number	Date	Plant	Slump	Spread	Air	Strengths	3 Day	7 Day	28 Day	56 Day	A
CL4KP	924149	11/5/2019	11 Seat	8.25		1.30	3650	4860	7630			
CL4KP	SF361	1/5/2020	11 Seat	7.50				7790	9640			
CL4KP	RC404574	1/8/2020	11 Seat	8.00				5210	7770			
CL4KP	RC404576	1/10/2020	11 Seat	8.25				4830	7530			
CL4KP	RC390188	1/13/2020	11 Seat	8.00				6850	9600			
CL4KP	rc390239	1/16/2020	11 Seat	8.00				6080	8730			
CL4KP	1562055	1/22/2020	11 Seat	8.00				4340	6630			
CL4KP	RC396685	1/22/2020	11 Seat	8.00				4340	6630			



# Concrete Mix Design

Contractor Project Wide All Contractors		Submitted By Adam Gaunt - Stoneway Concrete		Date 01/18/2021	
Concrete Supplier Stoneway Concrete			Plant Location Black River, Renton		
Contract Number 9242		Contract Name I405 Renton To Bellevue			

This mix is to be used in the following Bid Item No(s): \_\_\_\_\_

Concrete Class: Other - Define in Remarks

Remarks

Class 5000P

Recycled water to be used at 50% unless specified at time of order, extra charges may apply

Mix Design No. CL4KP

Plant No. 12

Cementitious Materials	Source	Plant	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Lafarge NA	Richmond, BC	ASTM C 595 Type IL(15)	3.15	600
Fly Ash <sup>a</sup>			<input type="checkbox"/> F <input type="checkbox"/> C Alkali % _____		
GGBFS (Slag) <sup>a</sup>	Lafarge NA	Seattle, WA	<input checked="" type="checkbox"/> 100 <input type="checkbox"/> 120	2.87	181

Concrete Admixtures	Manufacturer	Product	Est. Range (oz/cy)
Air Entrainment			
Water-Reducing Type A	GCP Applied Technologies	Zyla 630	1-50
Water-Reducing and Retarding Type D	GCP Applied Technologies	Recover	1-50

Water (Maximum) 312 lbs/cy

Is any of the water Recycled or Reclaimed? ☒ Yes<sup>d</sup> ☐ No

Water Cementitious Ratio (Maximum) 0.40

Mix Design Density (pcf) 147.1

## Design Performance (Attach Test Data)

Average 28-day compressive strength (psi) 7820

Average 14-day flexural strength (psi) (Concrete Pavement Only)

Concrete Chloride Ion Content (% by mass of cement) .0094

☐ Water Soluble ☒ Acid Soluble

## Agency Use Only (Check appropriate Box)

☒ This Mix Design MEETS CONTRACT SPECIFICATIONS and may be used on the bid items noted above

☐ This Mix Design DOES NOT MEET CONTRACT SPECIFICATIONS and is being returned for corrections

Reviewed By: \_\_\_\_\_

2/17/21

PE Signature

Date

Mix Design No. CL4KPPlant No. 12Aggregate Gradation ☒ AASHTO ☐ CombinedNominal Maximum Size (In) 3/8

Aggregates	1	2	3	4	5	Total
WSDOT Source No. <sup>b</sup>	A458	A458				
Source Expiration Date <sup>b</sup>	08/25/21	08/25/21				
ASR Expansion (%) <sup>b</sup> <input type="checkbox"/> 14 Day <input checked="" type="checkbox"/> 1 Year	.03	.03				
Is ASR Mitigation Required?	NO	NO				
Stock Pile Grading <sup>c</sup>	#8	Class 1				
Percent of Total Aggregate	53	47				100
Specific Gravity (SSD)	2.69	2.60				
Lbs/cy (ssd)	1551	1357				2908
<b>Include Percent Passing for each aggregate component. Include Total only for Combined Gradations.</b>	<b>Percent Passing</b>					<b>Total</b>
2 inch	100.00	100.00				100.00
1-1/2 inch	100.00	100.00				100.00
1 inch	100.00	100.00				100.00
3/4 inch	100.00	100.00				100.00
1/2 inch	100.00	100.00				100.00
3/8 inch	96.00	100.00				97.87
No. 4	16.00	100.00				55.20
No. 8	2.00	80.00				38.40
No. 16	1.00	59.00				28.07
No. 30	0.00	32.00				14.93
No. 50	0.00	10.00				4.67
No. 100	0.00	2.00				0.93
No. 200	0.00	1.00				0.47

Fineness Modulus: (Required for Class 2 Sand)

Proposed ASR Mitigation Method:

**Notes:**

- a Fly ash or GGBFS is required for Class 4000P mix.
- b Enter data from WSDOT ASA Database. ASR Mitigation is required for sources with 14-day expansions greater than 0.20%. No mitigation is required if the 1-year expansion is less than 0.04%. Proposed mitigation methods for 14-day expansions greater than 0.45% require ASTM C 1567 tests proving that the method is effective. See WSDOT Standard Specification 9-03.1.
- c Stockpile gradation: AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation stockpile sizes. See WSDOT Standard Specification 9-03.1.
- d Attach test results indicating conformance to Standard Specification 9-25.1.



# Concrete Mix Design

Contractor Project Wide All Contractors		Submitted By Adam Gaunt - Stoneway Concrete		Date 01/18/2021	
Concrete Supplier Stoneway Concrete			Plant Location Houser Way, Renton		
Contract Number 9242		Contract Name I405 Renton To Bellevue			

This mix is to be used in the following Bid Item No(s): \_\_\_\_\_

Concrete Class: Other - Define in Remarks

Remarks

Class 5000P

Recycled water to be used at 50% unless specified at time of order, extra charges may apply

Mix Design No. CL4KP

Plant No. 14

Cementitious Materials	Source	Plant	Type, Class or Grade	Sp. Gr.	Lbs/cy
Cement	Lafarge NA	Richmond, BC	ASTM C 595 Type IL(15)	3.15	600
Fly Ash <sup>a</sup>			<input type="checkbox"/> F <input type="checkbox"/> C Alkali % _____		
GGBFS (Slag) <sup>a</sup>	Lafarge NA	Seattle, WA	<input checked="" type="checkbox"/> 100 <input type="checkbox"/> 120	2.87	181

Concrete Admixtures	Manufacturer	Product	Est. Range (oz/cy)
Air Entrainment			
Water-Reducing Type A	GCP Applied Technologies	Zyla 630	1-50
Water-Reducing and Retarding Type D	GCP Applied Technologies	Recover	1-50

Water (Maximum) 312 lbs/cy

Is any of the water Recycled or Reclaimed? ☒ Yes<sup>d</sup> ☐ No

Water Cementitious Ratio (Maximum) 0.40

Mix Design Density (pcf) 147.1

## Design Performance (Attach Test Data)

Average 28-day compressive strength (psi) 7820

Average 14-day flexural strength (psi) (Concrete Pavement Only)

Concrete Chloride Ion Content (% by mass of cement) .0094

☐ Water Soluble ☒ Acid Soluble

## Agency Use Only (Check appropriate Box)

☒ This Mix Design MEETS CONTRACT SPECIFICATIONS and may be used on the bid items noted above

☐ This Mix Design DOES NOT MEET CONTRACT SPECIFICATIONS and is being returned for corrections

Reviewed By: \_\_\_\_\_

2/17/21

PE Signature

Date

Mix Design No. CL4KPPlant No. 14Aggregate Gradation ☒ AASHTO ☐ CombinedNominal Maximum Size (In) 3/8

Aggregates	1	2	3	4	5	Total
WSDOT Source No. <sup>b</sup>	A458	A458				
Source Expiration Date <sup>b</sup>	08/25/21	08/25/21				
ASR Expansion (%) <sup>b</sup> <input type="checkbox"/> 14 Day <input checked="" type="checkbox"/> 1 Year	.03	.03				
Is ASR Mitigation Required?	NO	NO				
Stock Pile Grading <sup>c</sup>	#8	Class 1				
Percent of Total Aggregate	53	47				100
Specific Gravity (SSD)	2.69	2.60				
Lbs/cy (ssd)	1551	1357				2908
<b>Include Percent Passing for each aggregate component. Include Total only for Combined Gradations.</b>	<b>Percent Passing</b>					<b>Total</b>
2 inch	100.00	100.00				100.00
1-1/2 inch	100.00	100.00				100.00
1 inch	100.00	100.00				100.00
3/4 inch	100.00	100.00				100.00
1/2 inch	100.00	100.00				100.00
3/8 inch	96.00	100.00				97.87
No. 4	16.00	100.00				55.20
No. 8	2.00	80.00				38.40
No. 16	1.00	59.00				28.07
No. 30	0.00	32.00				14.93
No. 50	0.00	10.00				4.67
No. 100	0.00	2.00				0.93
No. 200	0.00	1.00				0.47

Fineness Modulus: (Required for Class 2 Sand)

Proposed ASR Mitigation Method:

**Notes:**

- a Fly ash or GGBFS is required for Class 4000P mix.
- b Enter data from WSDOT ASA Database. ASR Mitigation is required for sources with 14-day expansions greater than 0.20%. No mitigation is required if the 1-year expansion is less than 0.04%. Proposed mitigation methods for 14-day expansions greater than 0.45% require ASTM C 1567 tests proving that the method is effective. See WSDOT Standard Specification 9-03.1.
- c Stockpile gradation: AASHTO No. 467, 57, 67, 7, 8; WSDOT Class 1, Class 2; or combined gradation stockpile sizes. See WSDOT Standard Specification 9-03.1.
- d Attach test results indicating conformance to Standard Specification 9-25.1.

Date: 1/18/2021



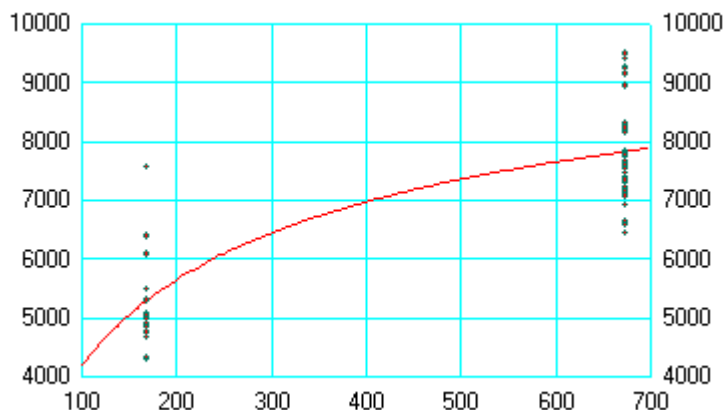
**Stoneway Concrete**  
Where Quality Counts

9216 8th AVENUE S  
SEATTLE, WA 98108  
OFFICE:(425)226-1000  
FAX:(425)228-4924

**Mix Name: CL4KP**

Units : US

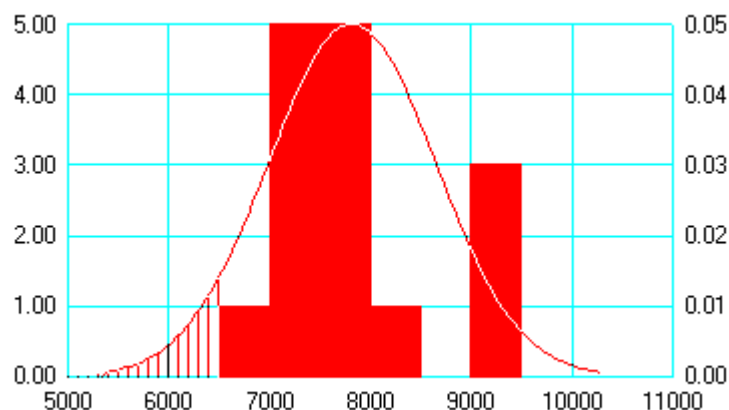
PSI Strength and Strength Fit vs Maturity



Maturity Hours

PSI # of Occ.

Histogram for 28 Day Strength



PSI

95% of tests lie above cross-hatched area

STRENGTH SUMMARY, Compression  
Strengths

Either 4" x 8" Or 6" x 12"

No. Of Tests	Avg Slump	Avg Air	Avg 3 Day	Avg 7 Day	Avg 28 Day	Avg 56 Day	Avg Acc Age	Accept Age
15	7.38	.00		5260	7820		7820	28

Std ACI318  
Dev Req'd  
-----  
590 6090

DETAILED STRENGTH, Compression

Either 4" x 8" Or 6" x 12"

Mix Number	Test Number	Date	Plant	Slump	Spread	Air	Strengths	3 Day	7 Day	28 Day	56 Day	A
CL4KP	999773	7/16/2019	14 Hous	5.00				6100	8240			
CL4KP	E238622	9/10/2019	14 Hous					7580	9200			
CL4KP	E238621	9/10/2019	14 Hous	8.00				5500	9390			
CL4KP	RC389815	1/6/2020	14 Hous	6.00				6400	9190			
CL4KP	RC404575	1/9/2020	14 Hous	7.50				5000	7730			
CL4KP	RC390242	1/14/2020	14 Hous	7.50				4870	7450			
CL4KP	RC390195	1/15/2020	14 Hous	8.00				4770	7200			
CL4KP	RC390241	1/17/2020	14 Hous	7.50				4690	7530			
CL4KP	RC396683	1/20/2020	14 Hous	7.50				5310	7730			
CL4KP	RC396684	1/21/2020	14 Hous	7.00				4920	7370			
CL4KP	RC396687	1/23/2020	14 Hous	7.50				4980	7480			
CL4KP	RC396689	1/24/2020	14 Hous	8.00				4330	7050			
CL4KP	RC396691	1/27/2020	14 Hous	7.50				5090	7510			
CL4KP	RC396693	1/28/2020	14 Hous	8.25				5060	7650			
CL4KP	RC396695	1/29/2020	14 Hous	8.00				4350	6570			

# National Ready Mixed Concrete Association



## **Certificate of Conformance For Concrete Production Facilities**

THIS IS TO CERTIFY THAT

***Seattle Plant, Seattle, WA***

***Stoneway Concrete***

has been inspected by the undersigned licensed professional engineer for conformance with the requirements of the *Check List for Ready Mixed Concrete Production Facilities*. As of the inspection date, the facilities met the requirements for production by

***Central Mixing with Automatic Batching and Recordings of  
Cementitious Materials, Aggregate, Water, and Chemical Admixtures***



A handwritten signature in black ink, reading "Robert G. Shogren", written over a horizontal line.

Signature of Licensed Professional Engineer

***August 18, 2020***

Inspection Date

***October 17, 2022***

Certification Expiration Date

This company will maintain these facilities in compliance with the *Check List* requirements and will correct promptly any deficiencies which develop.

A handwritten signature in black ink, reading "David A. Alston", written over a horizontal line.

Signature of Company Official

A handwritten signature in black ink, reading "Vice President", written over a horizontal line.

Title of Company Official

**NOTICE:** The Check List indicates only that plant facilities are satisfactory for the production of concrete when properly operated. Conformance of the concrete itself with specification requirements must be verified by usual inspection methods in accordance with sales agreements.

This certificate is issued by the National Ready Mixed Concrete Association on verification that the production facility conforms to the requirements of the NRMCA Certification of Ready Mixed Concrete Production Facilities, QC3. Unauthorized reproduction or misuse of this certificate may result in legal action.

Plant ID #: 801273

Certification ID #: 26403

© 1965, 1992, 2001, 2002, 2006, 2007, 2012

**National Ready Mixed Concrete Association 66 Canal Center Plaza, Suite 250 • Alexandria • Virginia 22314**



# National Ready Mixed Concrete Association



## **Certificate of Conformance For Concrete Production Facilities**

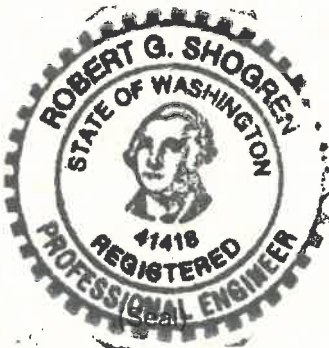
THIS IS TO CERTIFY THAT

***Houser Plant, Renton, WA***

***Stoneway Concrete***

has been inspected by the undersigned licensed professional engineer for conformance with the requirements of the *Check List for Ready Mixed Concrete Production Facilities*. As of the inspection date, the facilities met the requirements for production by

***Central Mixing with Automatic Batching and Recordings of  
Cementitious Materials, Aggregate, Water, and Chemical Admixtures***



Signature of Licensed Professional Engineer

***August 18, 2020***

Inspection Date

***October 17, 2022***

Certification Expiration Date

This company will maintain these facilities in compliance with the *Check List* requirements and will correct promptly any deficiencies which develop.

Signature of Company Official

Title of Company Official

**NOTICE:** The Check List indicates only that plant facilities are satisfactory for the production of concrete when properly operated. Conformance of the concrete itself with specification requirements must be verified by usual inspection methods in accordance with sales agreements.

This certificate is issued by the National Ready Mixed Concrete Association on verification that the production facility conforms to the requirements of the NRMCA Certification of Ready Mixed Concrete Production Facilities, QC3. Unauthorized reproduction or misuse of this certificate may result in legal action.

Plant ID #: 802812

Certification ID #: 26402

© 1965, 1992, 2001, 2002, 2006, 2007, 2012

**National Ready Mixed Concrete Association 66 Canal Center Plaza, Suite 250 • Alexandria • Virginia 22314**

# National Ready Mixed Concrete Association



## **Certificate of Conformance For Concrete Production Facilities**

THIS IS TO CERTIFY THAT

***Black River Plant, Renton, WA***

***Stoneway Concrete***

has been inspected by the undersigned licensed professional engineer for conformance with the requirements of the *Check List for Ready Mixed Concrete Production Facilities*. As of the inspection date, the facilities met the requirements for production by

***Central Mixing with Automatic Batching and Recordings of  
Cementitious Materials, Aggregate, Water, and Chemical Admixtures***



A handwritten signature in black ink, reading "Robert G. Shogren", written over a horizontal line.

Signature of Licensed Professional Engineer

***October 17, 2019***

Inspection Date

***December 23, 2021***

Certification Expiration Date

This company will maintain these facilities in compliance with the *Check List* requirements and will correct promptly any deficiencies which develop.

A handwritten signature in black ink, reading "David A. Alston", written over a horizontal line.

Signature of Company Official

***Vice President***

Title of Company Official

**NOTICE:** The Check List indicates only that plant facilities are satisfactory for the production of concrete when properly operated. Conformance of the concrete itself with specification requirements must be verified by usual inspection methods in accordance with sales agreements.

This certificate is issued by the National Ready Mixed Concrete Association on verification that the production facility conforms to the requirements of the NRMCA Certification of Ready Mixed Concrete Production Facilities, QC3. Unauthorized reproduction or misuse of this certificate may result in legal action.

Plant ID #: 815484

Certification ID #: 25157

© 1965, 1992, 2001, 2002, 2006, 2007, 2012

**National Ready Mixed Concrete Association 66 Canal Center Plaza, Suite 250 • Alexandria • Virginia 22314**



## Qualified Product List

### Product Information

**Manufacturer :** Ash Grove Cement Company, Seattle - WA

**Product Name :** Type IL(X) Blended Hydraulic Cement

**Standard Spec :** 9-01.2(1)B, Concrete - Blended Hydraulic Cement

**Product Description :** Blended Hydraulic Cement Type IL(X), Manufactured by Ash Grove Cement Co. - Seattle Plant, Seattle WA. Per WSDOT Standard Specification 9-01.2(1)B, the value of (X) shall be a minimum of 5% and a maximum of 15%.

**Product Restriction :**

**Acceptance Code :** 2525

**Code Description :** Acceptance based upon the cement Manufacturer's Mill Test Report number being shown on each concrete producer's certificate of compliance.

**Last Updated :** Jan 29, 2021

**Contractors with WSDOT** [Click here for Contractor Product Info Page](#)



February 11, 2021

RE: ASTM C595 IL (X) Cement

To whom it may concern:

This letter is to clarify Cement type IL(X) for Ashgrove cement, Currently with changing markets pushing to lower global warming potential numbers (GWP), The content for limestone is fluctuating during production, The goal is to reach the 15% limit to maximize c02 reduction. Limestone contents will remain within the spec limits for the duration of the project at 5-15% If any question of content is raised please refer to the most current production MillCert. At the time of this letter content has been raised from 10% to 13%

Please contact me if additional information is required at (206)786-8139

Sincerely,  
STONEWAY CONCRETE

Adam Gaunt  
Concrete Technical Services



# ASH GROVE CEMENT COMPANY



"WESTERN REGION"  
11811 N.E. First Street, Suite A310  
Bellevue, WA 98005  
Sales Office: (425) 688-0110  
Toll Free: 1-800-665-4382  
Fax: (425) 688-0122

January 11, 2021

Greg McKinnon  
Stoneway Concrete  
9216 8<sup>th</sup> Ave. S.  
Seattle, WA 98108

Dear Greg:

This letter is issued to certify that the cement we supply for your use is in conformance with the requirements of ASTM C-150 for Type I, II and III cement. We also certify that our Type IL cement meets the requirements of ASTM C595 and AASHTO M240 for Blended Hydraulic Cements. We further certify that our cement meets the requirements of the Washington DOT specification, FAA, Corp. of Engineers, and AASHTO M-85.

Attached you will find our Mill Analysis. We further certify that this cement meets all the requirements of the "Buy America Act."

If you should have any questions regarding the use of our product, please feel free to contact the undersigned.

Sincerely yours,



Dave Burg  
Technical Services Manager

Attachment



## Mill Test Report

Plant Seattle Cement Type IL(13) - Portland Limestone Cement  
 Production Period November 1, 2020 - December 1, 2020

Date 5-Jan-21  
 Certification No. IL 2020-9

### STANDARD REQUIREMENTS ASTM C 595 Tables 1, 2 and 3

CHEMICAL			PHYSICAL		
Item	Spec. Limit	Test Result	Item	Spec. Limit	Test Result
SiO <sub>2</sub> (%)	A	17.8	Air content of mortar (volume %)	12 max	4
Al <sub>2</sub> O <sub>3</sub> (%)	A	4.3	Blaine fineness (m <sup>2</sup> /kg)	A	495
Fe <sub>2</sub> O <sub>3</sub> (%)	A	3.1	% Passing 325 mesh	A	97.9
CaO (%)	A	63.9	Autoclave expansion (%)	-0.20 to 0.80	0.06
MgO (%)	A	0.8	Compressive strength MPa (PSI)	min:	
SO <sub>3</sub> (%) <sup>D</sup>	3.0 max	2.7	1 Day	A	19.9 (2880)
Ignition loss (%)	10.0 max	6.2	3 Days	13.0	33.2 (4820)
Na <sub>2</sub> O (%)	A	0.22	7 Days	20.0	38.3 (5560)
K <sub>2</sub> O (%)	A	0.32	28 Days	25.0	43.2 (6270) <sup>B</sup>
Insoluble residue (%)	A	0.41	Time of setting (minutes)		
CO <sub>2</sub> (%)	A	5.2	Vicat Initial not less than	45	105
Limestone (%)	>5 and ≤15	12.3	Final not more than	420	182
CaCO <sub>3</sub> in limestone (%)	70 min	97	C1038 mortar bar expansion (%)	E	0.003 <sup>F</sup>
Potential phase composition (%) <sup>C</sup>			Sulfate resistance, C1012 6-month exp (%)	0.10 max	0.09 <sup>F</sup>
C3S	A	57	Cement Density (g/cm <sup>3</sup> )	A	3.07 <sup>B</sup>
C2S	A	8			
C3A	A	6			
C4AF	A	9			
			Meets ASTM C1157 Type MS		

<sup>A</sup>Not applicable.

<sup>B</sup>Test result represents most recent value.

<sup>C</sup>Adjusted per C150 A1.6.

<sup>D</sup>It is permissible to exceed the max SO<sub>3</sub> provided the cement does not develop expansion exceeding 0.020% at 14 days by Method C1038.

<sup>E</sup>Required only if percent SO<sub>3</sub> exceeds the limit in Table 1, in which case the Test Method C1038 expansion shall not exceed 0.020% at 14 days.

<sup>F</sup>Test result for this production period not available. Most recent test result provided.

We certify that the above described cement, at the time of shipment, meets the chemical and physical requirements of the ASTM C595/C595M-19 specification.

Signature: \_\_\_\_\_

Edward C. Rafacz

Title: \_\_\_\_\_

Chief Chemist



## Qualified Product List

### Product Information

**Manufacturer :** Lafarge North America, Richmond - BC

**Product Name :** Type IL(X) Blended Hydraulic Cement

**Standard Spec :** 9-01.2(1)B, Concrete - Blended Hydraulic Cement

**Product Description :** (AASHTO M240, ASTM C595) Blended hydraulic cement type IL(X): Manufactured in Richmond, British Columbia. Distributed from Seattle, WA. Per WSDOT Standard Specification 9-01.2(4), the value of (X) shall be a minimum of 5% and a maximum of 15%

**Product Restriction :**

**Acceptance Code :** 2525

**Code Description :** Acceptance based upon the cement Manufacturer's Mill Test Report number being shown on each concrete producer's certificate of compliance.

**Last Updated :** Feb 3, 2016

**Contractors with WSDOT** [Click here for Contractor Product Info Page](#)





Cement

January 2021

Dear Sirs,

RE: **Lafarge Cements Certificate of Compliance (2021)**

This is to certify that the Lafarge cements produced at Richmond BC and Exshaw AB Plants comply with ASTM C-150 and AASHTO M-95 for Types I, II, III and V. The Type IT(LX)(SX) cement produced at Seattle, WA comply with ASTM C-595 and AASHTO M-240 specifications. The Type IL(X) cement produced in Richmond BC and Exshaw AB comply with ASTM C-595 and AASHTO M-240 specifications.

NewCem (ground granulated blast furnace slag) meets ASTM C-989 and AASTHO M-302 specifications.

Centralia, Sundance fly ash and Kamloops Class N Pumice meet the specifications of ASTM C-618 and AASHTO M-295.

Should you have any questions, please feel free to call me.

Sincerely,

A handwritten signature in black ink that reads 'Robt S. Shogren'.

Rob Shogren, PE, Ph.D.  
Technical Service Engineer  
Lafarge North America  
(206)-923-9953

**WESTERN REGION**

5400 West Marginal Way SW, Seattle, Washington 98106-1517  
Office: 206.923.0098 or 800.477.0100 Fax: 206.923.0388





## Qualified Product List

### Product Information

**Manufacturer :** Lafarge North America, Seattle - WA

**Product Name :** NewCem

**Standard Spec :** 9-23.10, Concrete Admix - Ground Granulated Blast Furnace Slag

**Product Description :** Ground granulated blast furnace slag: Manufactured - Lafarge North America, Seattle, WA; Distributed from Seattle, WA, Pasco, WA, Spokane, WA, and Vancouver, WA. The primary raw materials are originated in Japan.

**Product Restriction :**

**Acceptance Code :** 2530

**Code Description :** Acceptance shall be by receipt of a Manufacturer's Mill Test Report submitted with the concrete mix design.

**Last Updated :** Jan 16, 2018

**Contractors with WSDOT** [Click here for Contractor Product Info Page](#)



# Cement Test Report

Mill Test Report Number: SEA\_NEWCEM\_OCTOBER20  
 YEAR: 2020  
 MONTH: SEPTEMBER  
 PLANT: Seattle  
 CEMENT TYPE: NewCem Grade 100

## Reference Cement

<b>Fineness by Air Permeability</b> (m <sup>2</sup> /kg; ASTM C204)	419		
<b>Fineness by 45 µm (No. 325) Sieve</b> (% retain; ASTM C430)	2.6		
<b>Compressive Strength</b> (ASTM C109/C109 M)		<u>psi</u>	<u>Min Limit</u>
7-day	5,020		-
28-day	6,260		5,000
		<u>Actual</u>	<u>Limits</u>
<b>Total Alkalies (Na<sub>2</sub>O + 0.658 K<sub>2</sub>O)</b> (%, ASTM C114)	0.84		0.6-0.9

## Slag

<b>Fineness by Air Permeability</b> (m <sup>2</sup> /kg; ASTM C204)	519		
<b>Fineness by 45 µm (No. 325) Sieve</b> (% retain; ASTM C430)	4.5		
<b>Compressive Strength</b> (ASTM C109/C109 M)		<u>psi [Mpa]</u>	<u>SAI Limit</u>
28-day (Previous Month)	6260 [43.2]	104	95
<b>Specific Gravity</b> (Mg/m <sup>3</sup> ; ASTM C188)	2.87		
		<u>Actual</u>	<u>Max Limit</u>
<b>Air Content of Mortar</b> (%, ASTM C185)	5		12
<b>Sulfide Sulfur</b> (% S, ASTM C114)	0.8		2.5
<b>Sulfate Ion</b> (% as SO <sub>3</sub> , ASTM C114)	0.8		A
<b>Autoclave expansion</b> (%, CSA A3004-B5)	0.001		0.5
<b>Color Value L*</b>	77.4		

## Slag

CHEMICAL ANALYSIS	Percent
Silica Dioxide (SiO <sub>2</sub> ; ASTM C114)	32.8
Ferric Oxide (Fe <sub>2</sub> O <sub>3</sub> ; ASTM C114)	1.4
Aluminum Oxide (Al <sub>2</sub> O <sub>3</sub> ; ASTM C114)	13.3
Calcium Oxide (CaO; ASTM C114)	43.5
Sulfur Trioxide (SO <sub>3</sub> ; ASTM C114)	2.8
Magnesium Oxide (MgO; ASTM C114)	4.5
Potassium Oxide (K <sub>2</sub> O; ASTM C114)	0.25
Titanium Oxide (TiO <sub>2</sub> ; ASTM C114)	0.62
Loss on Ignition (L.O.I.; ASTM C114)	1.75
Total Alkalies	0.44
Inorganic Process Addition	6

<sup>A</sup> Not Applicable.

The ground granulated blast furnace slag complies with the current specification of the chemical physical requirement of ASTM C-989, AASHTO M-302 for grade 100 Ground Granulated Blast Furnace Slag (GGBFS) and and CSA A3001 Slag.  
 Slag source is JFE Mineral Company in Kurashiki City, Japan. NewCem is ground and manufactured in Seattle, WA.



Certified by:



Daniel Waldron  
 Quality Control Laboratory Supervisor

October 15, 2020



WSDOT MATERIALS LAB

01/21/2021

## Aggregate Source Approval Report

Owner: Glacier Northwest

Aggregate Source: PS-B-335

Lessee:

Known as: DuPont Pit

Located in: A part of Section 22 and 23 Section 23 T19N R1E

County: Pierce

## Remarks:

**Mineral Agg. and Surfacing:**

Test Date: 02/25/2020

Expiration Date: 02/25/2025

Absorption: 0.75

Apparent Sp. G.: 2.778

Bulk Sp. G. (SSD): 2.741

Bulk Sp. G.: 2.721

Deg: 76

LA: 12

**Remarks:**

Currently approved as a source of aggregate for:

ATB

Ballast

BST Crushed Cover Stone

BST Crushed Screenings

Crushed Surfacing Base Course

Crushed Surfacing Key Stone

Crushed Surfacing Top Course

Gravel Backfill for Foundation Class A

HMA Other Courses

HMA Wearing Course

Maintenance Rock

Permeable Ballast

Acceptance tests need to be performed as necessary.

**Aggregates for Concrete:**

Test Date: 03/09/2020

Expiration Date: 03/09/2025

ASR - 14 Day :

ASR - One Year: 0.031

CCA Absorption: 0.82

CCA Sp.G: 2.701

Deg: 61

FCA Absorption: 1.48

FCA Organics: 1

FCA Sp. G: 2.668

LA: 11

**Remarks:** 1-Year ASR Results Expire 02/01/2022

Currently approved for:

Coarse Concrete Aggregates

Fine Concrete Aggregates

Acceptance tests need to be performed as necessary Acceptance tests need to be performed as necessary

**Riprap, Quarry Spalls, Rock for Rock Wall, Erosion and Scour Protection:**

Test Date:

Expiration Date:

Absorption:

Apparent Sp. G.:

Bulk Sp. G. (SSD):

Bulk Sp. G.:

Deg:

LA:

**Remarks:**

NOT Approved for:

Quarry Spalls	Riprap	Rock for Erosion and Scour Protection
Rock for Rock Walls	Stone 9-27.3(6)	

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<b>Streambed Aggregates:</b>	Test Date: 02/25/2020	Expiration Date: 02/25/2025
Absorption: 0.75	Apparent Sp. G.: 2.778	Bulk Sp. G. (SSD): 2.741      Bulk Sp. G.: 2.721
Deg: 76	LA: 12	

**Remarks:**

Currently Approved for:

Streambed Aggregate

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<b>Gravel Borrow for Structural Earth Walls:</b>	Test Date: 02/25/2020	Expiration Date: 02/25/2025
Bulk Sp. G. (SSD): 2.741	Deg: 76	LA: 12

**Remarks:** For geosynthetic reinforcement, the gravel borrow shall be tested for pH prior to placement. For metallic reinforcement, the gravel borrow shall be tested for pH, resistivity, chlorides, and sulfates prior to placement. If the resistivity of the backfill material equals or exceeds 5,000 ohm-cm, the specified chloride and sulfate limits may be waived. If the aggregate source has variable quality, additional testing may be required. Contact the Regional Materials Engineer or the State Geotechnical Engineer for direction.

Currently Approved for:

Gravel Borrow for Str Earth Walls

**ALL OTHER PIT RUN MATERIALS:**

Project Engineer may request preliminary samples but Aggregate Source Approval is not required.

**AGGREGATE MATERIALS NOT REQUIRING ASA APPROVAL :**

Aggregate for Gravel Base 9-03.10  
 Gravel Backfill for Foundation Class B 9-03.12(1)B  
 Gravel Backfill for Walls 9-03.12(2)  
 Gravel Backfill for Pipe Zone Bedding 9-03.12(3)  
 Gravel Backfill for Drains 9-03.12(4)  
 Gravel Backfill for Drywells 9-03.12(5)  
 Backfill for Sand Drains 9-03.13  
 Sand Drainage Blanket 9-03.13(1)  
 Gravel Borrow 9-03.14(1)  
 Select Borrow 9-03.14(2)

Common Borrow 9-03.14(3)

Native Material for Trench Backfill 9-03.15

Foundation Material Class A and B 9-03.17

Foundation Material Class C 9-03.18

Bank Run Gravel for Trench Backfill 9-03.19

Commercial Concrete Aggregate 6-02.3(2)B





## WSDOT MATERIALS LAB

01/21/2021

## Aggregate Source Approval Report

Owner: Quality Aggregates LLC

Aggregate Source: PS-A-458

Lessee:

Known as: Lake Francis Pit

Located in: NW 1/4 SE 1/4 Section 33 T23N R6E

County: King

## Remarks:

**Mineral Agg. and Surfacing:**

Test Date: 08/11/2016

Expiration Date: 08/11/2021

Absorption: 0.97

Apparent Sp. G.: 2.758

Bulk Sp. G. (SSD): 2.712

Bulk Sp. G.: 2.686

Deg: 76

LA: 17

**Remarks:**

Currently approved as a source of aggregate for:

ATB

Ballast

BST Crushed Cover Stone

BST Crushed Screenings

Crushed Surfacing Base Course

Crushed Surfacing Key Stone

Crushed Surfacing Top Course

Gravel Backfill for Foundation Class A

HMA Other Courses

HMA Wearing Course

Maintenance Rock

Permeable Ballast

Acceptance tests need to be performed as necessary.

**Aggregates for Concrete:**

Test Date: 08/25/2016

Expiration Date: 08/25/2021

ASR - 14 Day : 0.46

ASR - One Year: 0.03

CCA Absorption: 0.69

CCA Sp.G: 2.734

Deg: 77

FCA Absorption: 1.65

FCA Organics: 2

FCA Sp. G: 2.669

LA: 14

**Remarks:** 1-Year ASR results expire 04/19/2023

Currently approved for:

Coarse Concrete Aggregates

Fine Concrete Aggregates

Acceptance tests need to be performed as necessary Acceptance tests need to be performed as necessary

**Riprap, Quarry Spalls, Rock for Rock Wall, Erosion and Scour Protection:**

Test Date:

Expiration Date:

Absorption:

Apparent Sp. G.:

Bulk Sp. G. (SSD):

Bulk Sp. G.:

Deg:

LA:

**Remarks:**

NOT Approved for:

Quarry Spalls	Riprap	Rock for Erosion and Scour Protection
Rock for Rock Walls	Stone 9-27.3(6)	

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<b>Streambed Aggregates:</b>	Test Date: 08/25/2016	Expiration Date: 08/25/2021	
Absorption: 0.69	Apparent Sp. G.: 2.767	Bulk Sp. G. (SSD): 2.734	Bulk Sp. G.: 2.715
Deg: 77	LA: 14		

**Remarks:**

Currently Approved for:

Streambed Aggregate

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<b>Gravel Borrow for Structural Earth Walls:</b>	Test Date: 08/25/2016	Expiration Date: 08/25/2021
Bulk Sp. G. (SSD): 2.734	Deg: 77	LA: 14

**Remarks:** For geosynthetic reinforcement, the gravel borrow shall be tested for pH prior to placement. For metallic reinforcement, the gravel borrow shall be tested for pH, resistivity, chlorides, and sulfates prior to placement. If the resistivity of the backfill material equals or exceeds 5,000 ohm-cm, the specified chloride and sulfate limits may be waived. If the aggregate source has variable quality, additional testing may be required. Contact the Regional Materials Engineer or the State Geotechnical Engineer for direction.

Currently Approved for:

Gravel Borrow for Str Earth Walls

**ALL OTHER PIT RUN MATERIALS:**

Project Engineer may request preliminary samples but Aggregate Source Approval is not required.

**AGGREGATE MATERIALS NOT REQUIRING ASA APPROVAL :**

Aggregate for Gravel Base 9-03.10  
Gravel Backfill for Foundation Class B 9-03.12(1)B  
Gravel Backfill for Walls 9-03.12(2)  
Gravel Backfill for Pipe Zone Bedding 9-03.12(3)  
Gravel Backfill for Drains 9-03.12(4)  
Gravel Backfill for Drywells 9-03.12(5)  
Backfill for Sand Drains 9-03.13  
Sand Drainage Blanket 9-03.13(1)  
Gravel Borrow 9-03.14(1)  
Select Borrow 9-03.14(2)

Common Borrow 9-03.14(3)

Native Material for Trench Backfill 9-03.15

Foundation Material Class A and B 9-03.17

Foundation Material Class C 9-03.18

Bank Run Gravel for Trench Backfill 9-03.19

Commercial Concrete Aggregate 6-02.3(2)B



## Qualified Product List

### Product Information

**Manufacturer :** GCP Applied Technologies - Formerly W.R. Grace and Company, Vancouver - BC

**Product Name :** Recover

**Standard Spec :** 9-23.6(5), Concrete Admixture - Type D - Water-Reducing and Retarding Admixtures

**Product Description :** Liquid water reducing/set retarding admixture for concrete: Type D

**Product Restriction :**

**Acceptance Code :** 2250

**Code Description :** Acceptance is by field verification and the retaining of the Concrete Producer's Certificate of Compliance indicating the product and dosage of the admixture conform to the concrete mix design.

**Last Updated :** Aug 20, 2019

**Contractors with WSDOT** [Click here for Contractor Product Info Page](#)

# RECOVER®

Hydration stabilizer ASTM C494 Type B and D

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## Product Description

RECOVER® is a ready-to-use aqueous solution of chemical compounds specifically designed to stabilize the hydration of Portland cement concretes. The ingredients are factory pre-mixed in exact proportions under strict quality control to provide uniform results. One gallon weighs approximately 9.6 lbs (1.15 kg/L).

## Product Advantages

- Eliminates the need to discharge wash water from the mixer
- Prevents the waste of unused concrete
- Provides predictable extended set for continuous placement on mass concrete and tremie projects, or on long hauls to remote sites

## Uses

RECOVER® is used to stabilize mixer wash water and returned or leftover concrete for extended periods, allowing for use of the materials when specified or allowed. It is also used where controlled extended set of concrete is needed. It is the concrete user's responsibility to determine if leftover, returned or extended-set concrete is specified or allowed.

### Wash Water

For wash water applications, RECOVER® is used to eliminate the need to discharge wash water from the mixer. This allows the wash water to be used as mix water in the next batch of concrete produced and prevents the residual plastic concrete from hardening. Stabilization of up to 96 hours is possible depending on dosage rate.

### Returned Concrete

For returned or leftover concrete, RECOVER® is used to prevent plastic concrete from reaching initial set. This allows the concrete to be stored in a plastic state and then used when specified or allowed. The use of this concrete may require the addition of freshly batched concrete and/or an accelerator such as DARACCEL® or POLARSET®.

Stabilization of concrete for up to 96 hours is possible depending on dosage rate. Use prevents the waste of unused concrete.

### Set Time Control

RECOVER® is also used in situations where a controlled set time extension is required. Examples include: extended hauls, large continuous pours or pre-batching of concrete for later use.

## Addition Rates

Addition rates of RECOVER® for wash water range from 6 to 128 fl oz (180 to 3800 mL) per treatment. The amount used will depend on the specific materials involved, mixer type and stabilization period. Addition rates for returned or leftover concrete will range from 3 to 128 fl oz/100 lbs (195 to 8350 mL/100 kg) of cement. The amount used will depend on the specific materials involved, concrete age, temperature conditions and stabilization period. For applications requiring set time extensions well in excess of 4 hours, RECOVER® may be used at addition ranges from 5 to 50 oz/100 lbs (325 to 3260 mL/100 kg) of cement. For use as a traditional ASTM Type B or D retarder, RECOVER® may be used at addition rates of 2 to 6 oz/100 lbs (130 to 390 mL /100 kg) of cement. Proper dosage rate selection can only be achieved through pretesting. Consult your local GCP Applied Technologies admixture representative.

## Compatibility with Other Admixtures and Batch Sequencing

RECOVER® is compatible with most GCP admixtures as long as it is added separately to the concrete mix, usually through the water holding tank discharge line. In general, it is recommended that RECOVER® be added to the concrete mix near the end of the batch sequence for optimum performance. Different sequencing may be used if local testing shows better performance. Please see GCP Technical Bulletin TB-0110, *Admixture Dispenser Discharge Line Location and Sequencing for Concrete Batching Operations* for further recommendations.

Pretesting of the concrete mix should be performed before use, as conditions and materials change in order to ensure compatibility, and to optimize dosage rates, addition times in the batch sequencing and concrete performance. For concrete that requires air entrainment, the use of an ASTM C260 air entraining agent (such as Daravair® or Darex® product lines) is recommended to provide suitable air void parameters for freeze-thaw resistance. Please consult your GCP Applied Technologies representative for guidance.

## Packaging & Handling

RECOVER® is available in bulk, delivered by metered tank trucks, totes and drums.

RECOVER® will freeze, but will return to full effectiveness after thawing and thorough mechanical agitation.

## Performance

RECOVER® stabilizes the hydration process of Portland cement preventing it from reaching initial set. This stabilization is not permanent and is controlled by dosage rate. For wash water, the RECOVER® treated water is mixed or sprayed in a specific manner to thoroughly coat the interior of the mixer. The water is used as mix water in the next batch of concrete produced, which then scours the unhardened material from the interior of the mixer. Stabilization of returned or leftover concrete with RECOVER® maintains the plasticity of the concrete for the desired storage duration. This stabilized concrete then resumes normal hydration when the RECOVER® dosage effects subside, or when it is activated by the addition of fresh concrete and/or an accelerator. The result can be concrete with normal plastic and hardened properties.

## Dispensing Equipment

A complete line of GCP dispensing equipment is available for RECOVER<sup>®</sup>. This includes the Reach 360TM System which uses an innovative spray wand technology to simplify wash water procedures.

**gcpat.com | North America Customer Service: 1 877-4AD-MIX1 (1 877-423-6491)**

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Last Updated: 2018-08-24

**[gcpat.com/solutions/products/recover](http://gcpat.com/solutions/products/recover)**





## Qualified Product List

### Product Information

**Manufacturer :** GCP Applied Technologies - Formerly W.R. Grace and Company, Vancouver - BC

**Product Name :** Zyla 630

**Standard Spec :** 9-23.6(2), Concrete Admixture - Type A - Water-Reducing Admixtures

**Product Description :** Liquid normal range water reducing admixture for concrete: Type A

**Product Restriction :**

**Acceptance Code :** 2250

**Code Description :** Acceptance is by field verification and the retaining of the Concrete Producer's Certificate of Compliance indicating the product and dosage of the admixture conform to the concrete mix design.

**Last Updated :** Aug 20, 2019

**Contractors with WSDOT Click here for** [Contractor Product Info Page](#)

# ZYLA<sup>®</sup> 630

Water-reducing admixture -- ASTM C494 Type A and D

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## Product Description

ZYLA<sup>®</sup> 630 water-reducing admixture is a proprietary formulation incorporating highly purified specialty organic chemicals. ZYLA<sup>®</sup> 630 promotes more complete hydration of Portland cement and has no effect on concrete air entrainment.

The ZYLA<sup>®</sup> product line of water reducers is specially formulated to have a synergistic effect with polycarboxylate-based mid-range and high-range water reducers that improve flat-work finishability. This product contains no intentionally added chloride and as such is essentially chloride free. It is manufactured under rigid controls that provide uniform, predictable performance. ZYLA<sup>®</sup> 630 is supplied as a light brown, low viscosity liquid, and is ready-to-use as received. One gallon weighs approximately 9.1 lbs (1.1 kg/L).

## Product Advantages

- No impact on concrete air content
- Better control of water reduction and setting times as compared to traditional lignin-based water reducers
- Synergistic performance of polycarboxylate-based mid-range and high-range water reducers, which includes water reduction, concrete strength and air control
- In the hardened state, improves the compressive and flexural strengths at all ages of concrete versus traditional lignin-based water reducers

## Uses

ZYLA<sup>®</sup> 630 is used to produce concrete mixes with lower water content (typically 3% to 10% reduction), greater plasticity and higher compressive strengths. ZYLA<sup>®</sup> 630 is suitable for normal weight and light weight concrete in ready-mix, precast and prestressed applications.

## Finishability

The unique chemistry of ZYLA<sup>®</sup> 630 positively impacts the finishability of concrete by providing a creamier and more homogenous texture, with more uniform bleed rate relative to traditional lignin-based water reducers. The influence of ZYLA<sup>®</sup> 630 on the finishability of lean mixes has been particularly noticeable. Floating and troweling, by machine or hand, imparts a smooth, close tolerance surface.

## Addition Rates

The addition rate range of 3 to 5 fl oz/100 lbs (195 to 325 mL/ 100 kg) of cement or cementitious is typical for most applications. However addition rates of 2 to 7 fl oz/100 lbs (130 to 455 mL/100 kg) of cement or cementitious may be used if local testing shows acceptable performance. Pretesting is required to determine the appropriate addition rate for desired performance. The optimum addition rate depends on the other concrete mixture components, job conditions, and desired performance characteristics.

## Compatibility with Other Admixtures and Batch Sequencing

ZYLA® 630 is compatible with most GCP admixtures as long as they are added separately to the concrete mix, usually through the water holding tank discharge line. In general, it is recommended that ZYLA® 630 be added to the concrete mix near the end of the batch sequence for optimum performance. Different sequencing may be used if local testing shows better performance. Please see GCP Technical Bulletin TB-0110, *Admixture Dispenser Discharge Line Location and Sequencing for Concrete Batching Operations* for further recommendations.

Pretesting of the concrete mix should be performed before use, as conditions and materials change in order to assure compatibility, and to optimize dosage rates, addition times in the batch sequencing and concrete performance. For concrete that requires air entrainment, the use of an ASTM C260 air-entraining agent (such as DARAVAIR® or DAREX® product lines) is recommended to provide suitable air void parameters for freeze-thaw resistance. Please consult your GCP Applied Technologies representative for guidance.

## Packaging & Handling

ZYLA® 630 is available in bulk, delivered by metered tank trucks, in totes, and in drums.

ZYLA® 630 will freeze at about 28°F (-2°C), but will be completely uniform after thawing and thorough agitation.

## Dispensing Equipment

A complete line of accurate, automatic dispensing equipment is available. ZYLA ® 630 may be introduced to the mix through the water holding tank discharge line. The ZYLA® product line is formulated to be free of sediment.

## Specifications

Concrete shall be designed in accordance with *Standard Recommended Practice for Selecting Proportions for Concrete*, ACI 211.

The water-reducing admixture shall be ZYLA ® 630, as manufactured by GCP Applied Technologies, or equal. The admixture shall not contain calcium chloride as a functional ingredient. ZYLA® 630 will not promote corrosion of reinforcing steel embedded in concrete. It shall be used in strict accordance with the manufacturers' recommendations. The admixture shall comply with ASTM Designation C494, Type A and D water-reducing admixtures. Certification of compliance shall be made available on request.

The admixture shall be delivered as a ready-to-use liquid product and shall require no mixing at the batching plant or job site.

**gcpat.com | North America Customer Service: 1 877-4AD-MIX1 (1 877-423-6491)**

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Last Updated: 2018-08-24

**[gcpat.com/solutions/products/zyla-water-reducing-admixtures/zyla-630](http://gcpat.com/solutions/products/zyla-water-reducing-admixtures/zyla-630)**

**I-405 / Renton to Bellevue Widening and Express Toll Lanes Project Design Build Project  
Review Comment Summary and Resolution Form**

Package Description: RAM0171 Stoneway Conc Mix Design CL4KP 5K						Submittal Date: 2/4/2021		
Reviewer(s): Nancy Guinn / WSDOT						Comment Due Date: 2/9/2021		
Comment		Sheet No.	Review Comment	Initial Code	Response	Response By	Final Code	Correction Verified by
No.	By	*		**			***	
Code: A=Accept Comment; B=Review and Discuss Comment; C=Evaluated but Not Incorporated; D=Comment Beyond Scope or Beyond Design Phase								
Note: * Indicates Sheet No., Page No. and Line No. or "G" for General Comment; ** Filled out by Design; *** Agreed Resolution (code "B" is not acceptable)								
1	NG	RAM Page 1 and MD CL4KP from Seattle Plant 11	Fourth Material Item: Ashgrove Cement Type IL(10) - MD CL4KP from Seattle notes Ashgrove Cement Type IL(10) but the MTR attached to submittal is for Ashgrove Cement Type IL(13) - need MTR for Ashgrove Cement Type IL(10) or change RAM and Mix Design to Type IL(13)	A	RAM cover sheet and mix design form have been updated to say Ashgrove Cement Type IL(X). X fluctuates within the WSDOT Standard Specification allowable 5-15%. A letter from Stoneway has been added to the RAM to clarify variabe limestone content in Ashgrove cement.	IA (Stoneway)		
2	BW	RAM Pg - 17.	I believe this mill test report is intended for test results for the Cement Type IL(10) that is submitted with this RAM, but the mill test report shows that it's for Cement Type IL(13). Needs to be a Mill test report for the Cement Type IL(10).	A	Addressed per comment #1	IA (Stoneway)		
1	NG	RAM Page 1	Fourth Material Item: Under Material delete "Limestone 5-15"					
2	NG	RAM Page 1	Fourth Material Item: Under RAM Approval Code change 2 to 2* and under <b>Remarks:</b> add *See attached Stoneway letter dated February 11, 2021 regarding Mill Cert designation for Ashgrove Cement"					

**I-405 / Renton to Bellevue Widening and Express Toll Lanes Project Design Build Project  
Review Comment Summary and Resolution Form**

<b>Package Description:</b> RAM0171 Stoneway Conc Mix Design CL4KP 5K						<b>Submittal Date:</b> 2/4/2021		
<b>Reviewer(s):</b> Nancy Guinn / WSDOT						<b>Comment Due Date:</b> 2/9/2021		
Comment		Sheet No.	Review Comment	Initial Code	Response	Response By	Final Code	Correction Verified by
No.	By	*						
<b>Code:</b> A=Accept Comment; B=Review and Discuss Comment; C=Evaluated but Not Incorporated; D=Comment Beyond Scope or Beyond Design Phase <b>Note:</b> * Indicates Sheet No., Page No. and Line No. or "G" for General Comment; ** Filled out by Design; *** Agreed Resolution (code "B" is not acceptable)								
1	NG	RAM Page 1 and MD CL4KP from Seattle Plant 11	Fourth Material Item: Ashgrove Cement Type IL(10) - MD CL4KP from Seattle notes Ashgrove Cement Type IL(10) but the MTR attached to submittal is for Ashgrove Cement Type IL(13) - need MTR for Ashgrove Cement Type IL(10) or change RAM and Mix Design to Type IL(13)					
2	BW	RAM Pg - 17.	I believe this mill test report is intended for test results for the Cement Type IL(10) that is submitted with this RAM, but the mill test report shows that it's for Cement Type IL(13). Needs to be a Mill test report for the Cement Type IL(10).					